

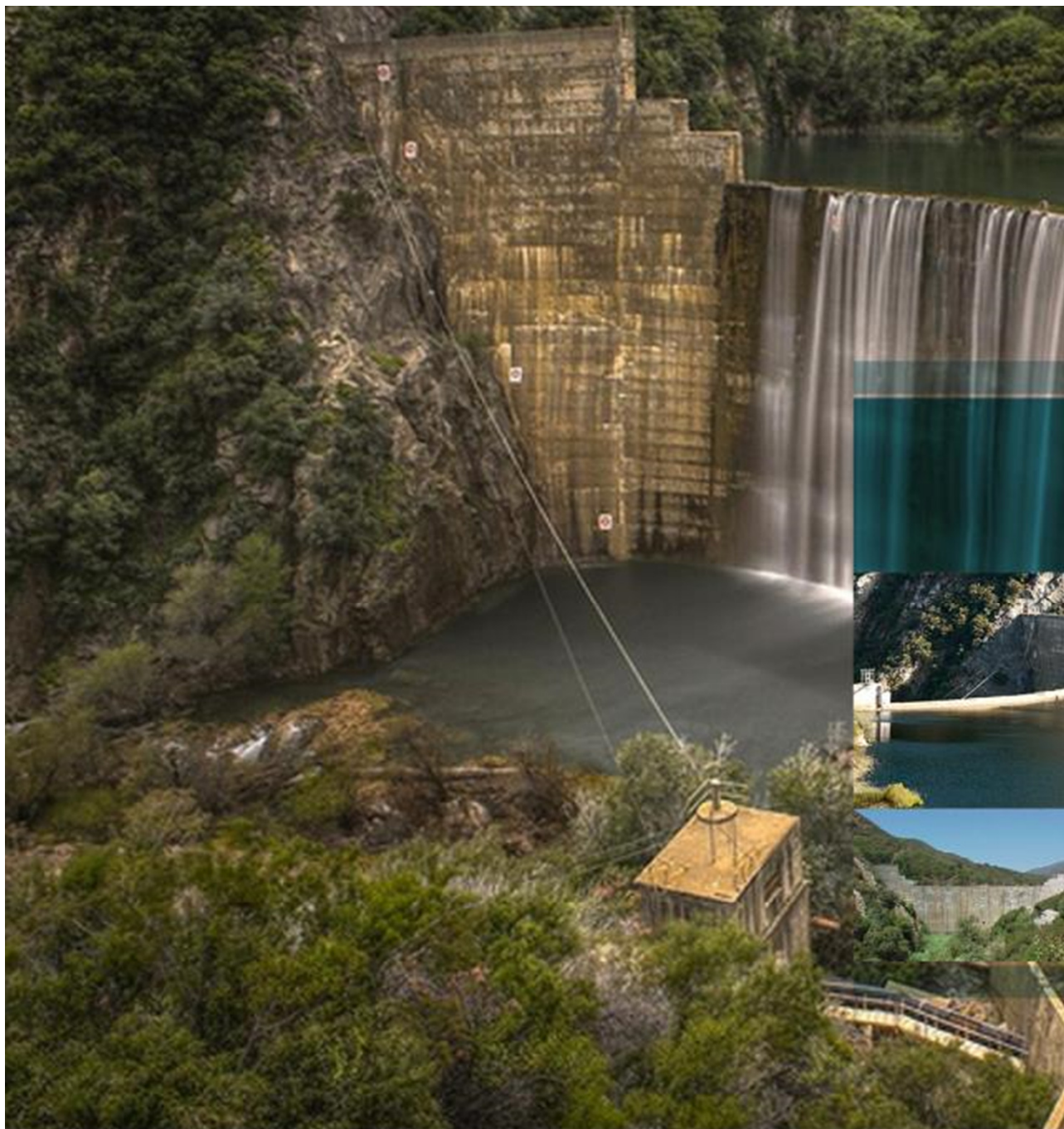


***Tasks 2.1 and 2.2 : Hydrology
& Sediment Characterization
May 28, 2014***

PRESENTATION

MATILIJA DAM

DAM REMOVAL PLANS AND SEDIMENT TRANSPORT
ANALYSIS AND ROBLES DIVERSION MITIGATION



Topics

1. Watershed hydrology
2. Impoundment-area sediment
3. Watershed sediment
4. Questions



MATILIJA DAM
DAM REMOVAL PLANS AND SEDIMENT TRANSPORT ANALYSIS AND ROBLES DIVERSION MITIGATION



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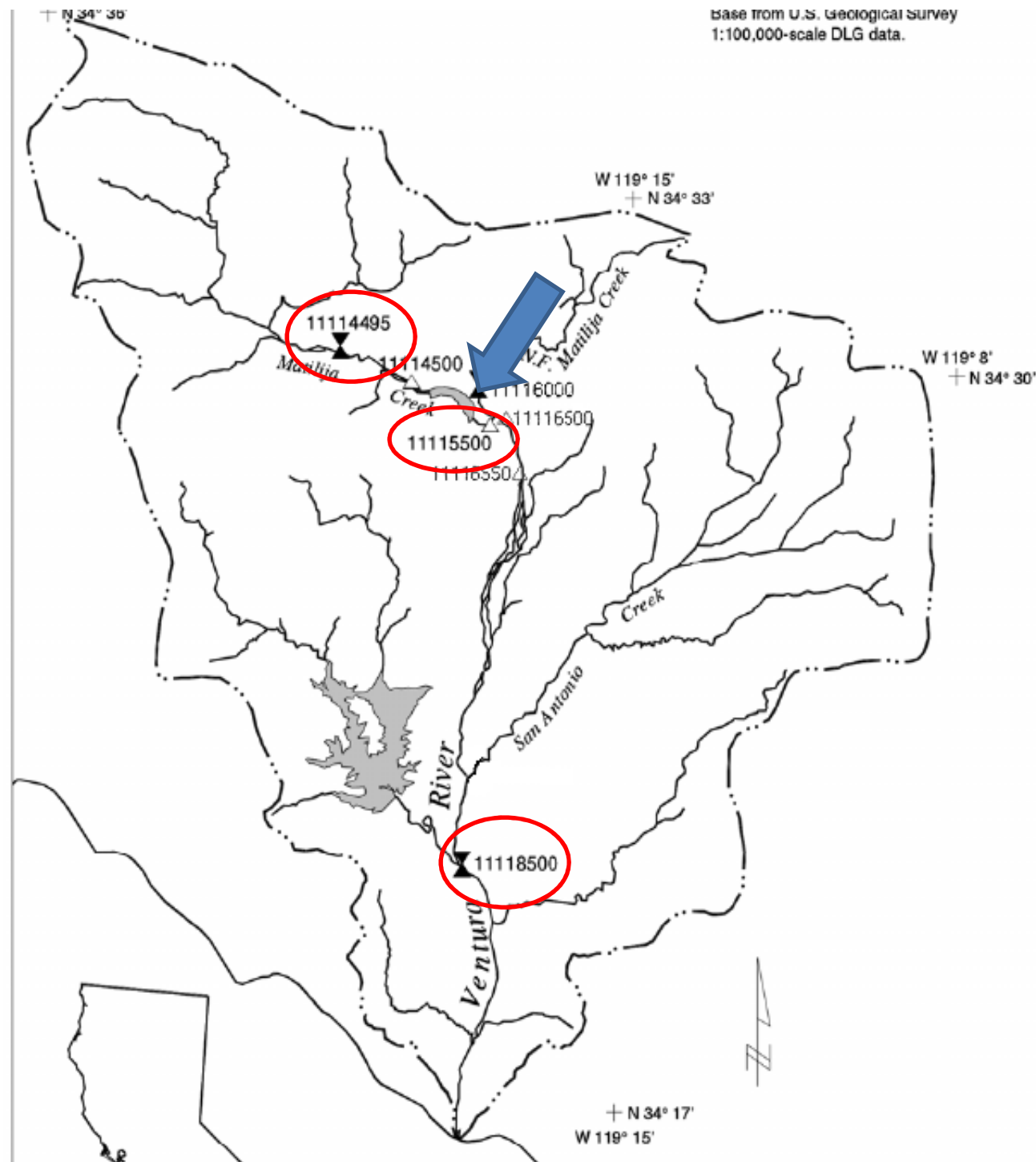


MATILIJA DAM
DAM REMOVAL PLANS AND SEDIMENT TRANSPORT ANALYSIS AND ROBLES DIVERSION MITIGATION



Table 1. USGS flow gages and dates of record in the Ventura River watershed.

[illegible]



But first...a quick tour of the channel, from above
Matilija Dam to Ventura River gage 11118500































Ventura River at Foster Park (gage 11118500)



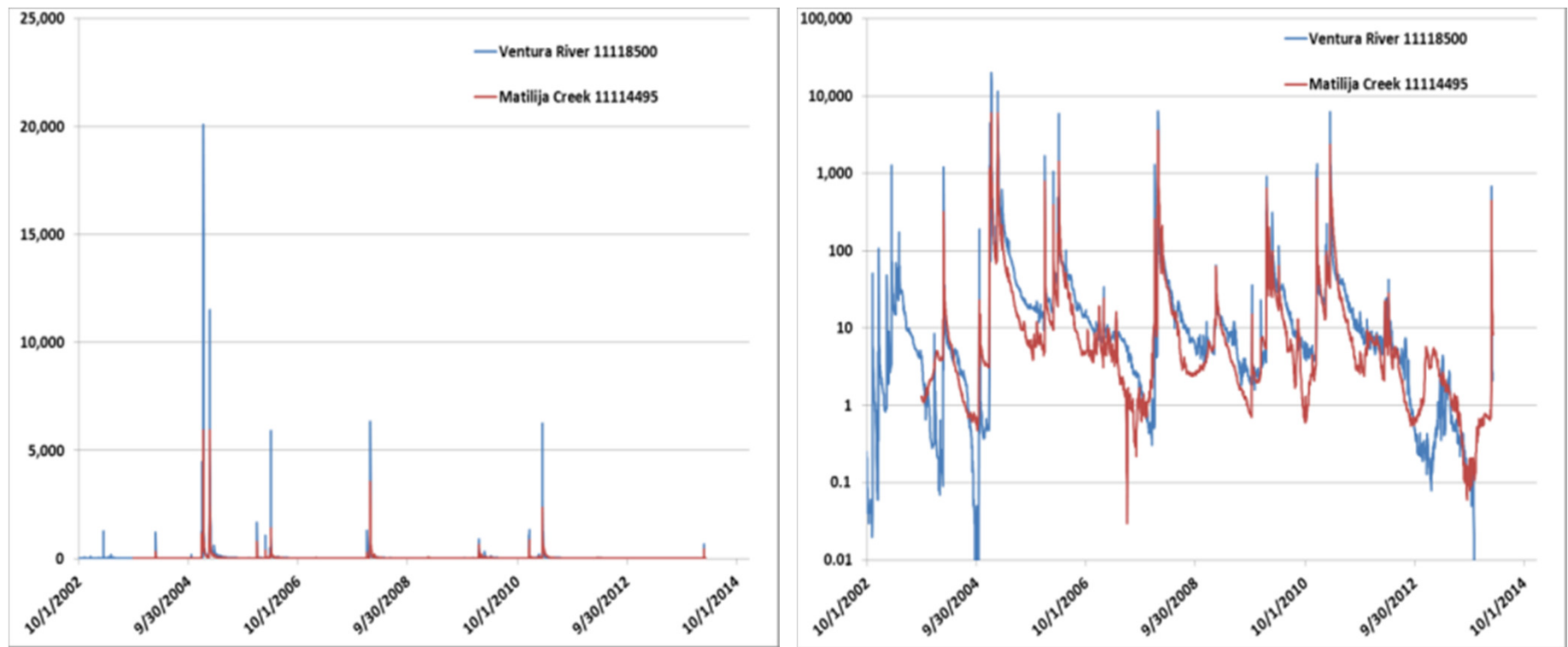


Figure 2. Hydrographs of the Ventura River and Matilija Creek for water years 2003 through mid-2014, expressed as cubic feet per second (cfs) on arithmetic (left) and log (right) scales. The former emphasizes the dramatic variability of this system, with individual flow events of typically a few days' to a few weeks' duration, separated by one to several years of very low flow; the latter shows that that flow is minimal but almost always non-zero in both channels at the gage locations. Both graphs also show the close correspondence of tributary (Matilija) and mainstem (Ventura) flows at the resolution of a daily time step.

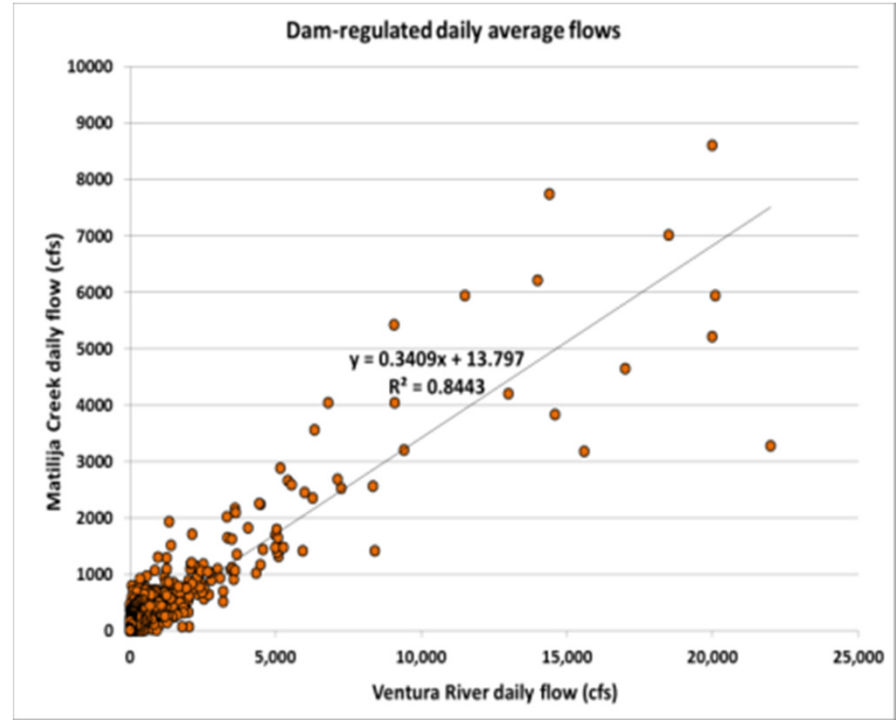
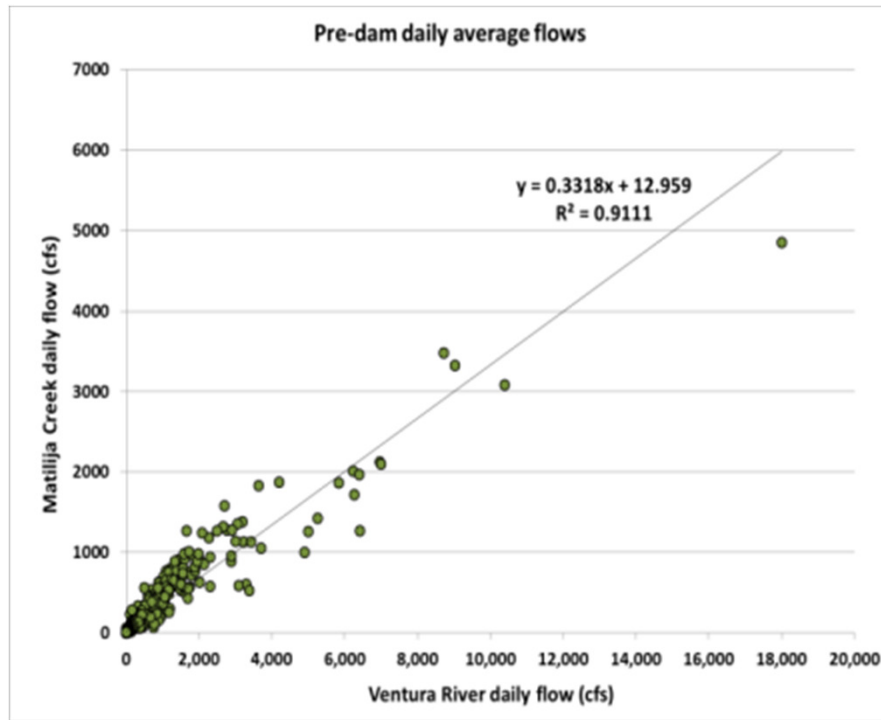


Figure 3. Same-day average flows for the Ventura River at gage 11118500 (x axis) and Matilija Creek (y axis) for the pre-dam (left) and dam-regulated (i.e., post- 4/14/1948) (right) periods. Correlations suggest:

1. a **3:1 ratio of flows** , and
2. **no significant systematic differences between the two periods.**

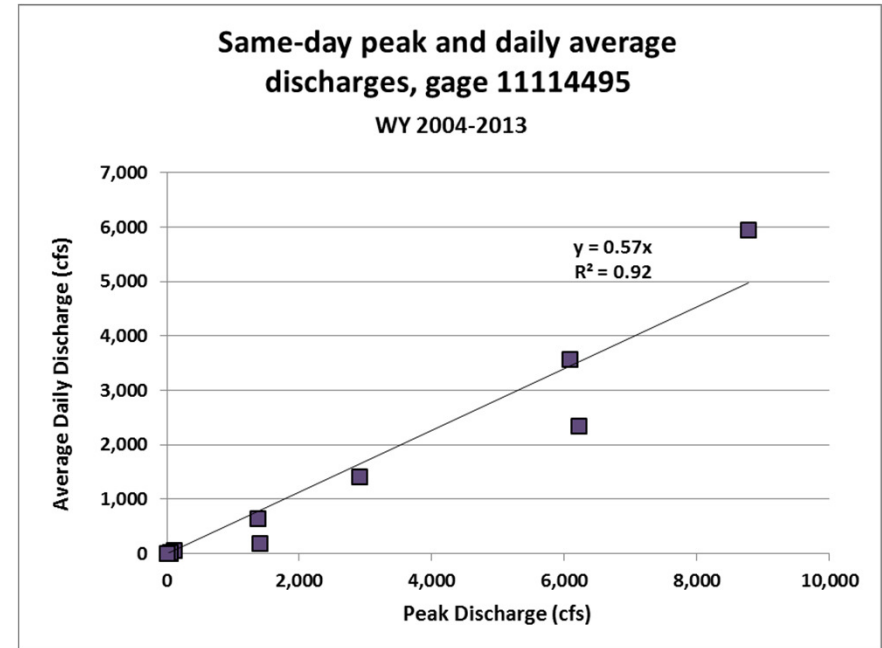
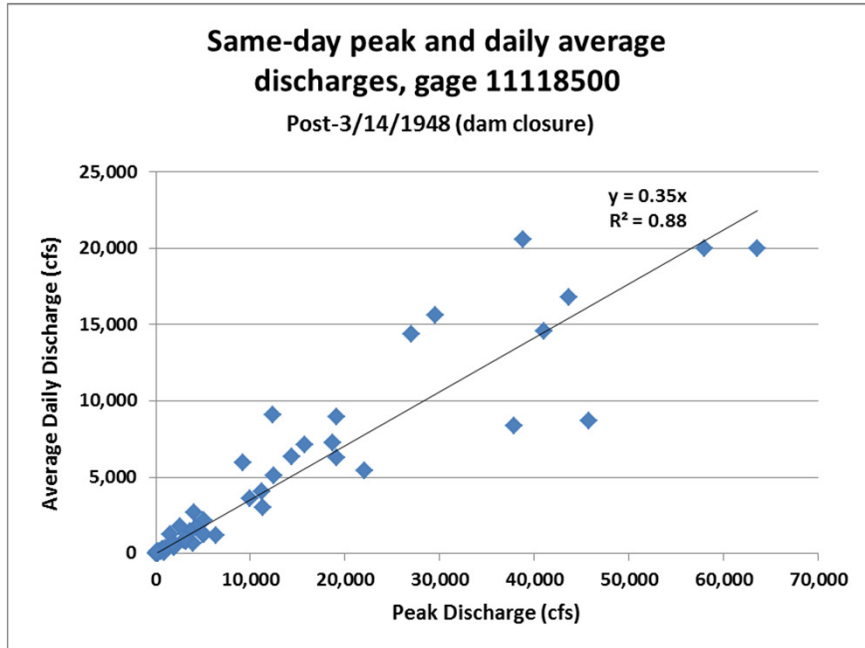


Figure 4. Same-day peak and daily average flows for the annual flood on the Ventura River (left, gage 11118500) and Matilija Creek (right, gage 11114495) for the dam-regulated period. **Correlations suggest an average daily flow of about 35% of the same-day instantaneous peak flow on the Ventura River** (but with a range from 19-73% for individual events >10,000 cfs) **and 57% on Matilija Creek.**

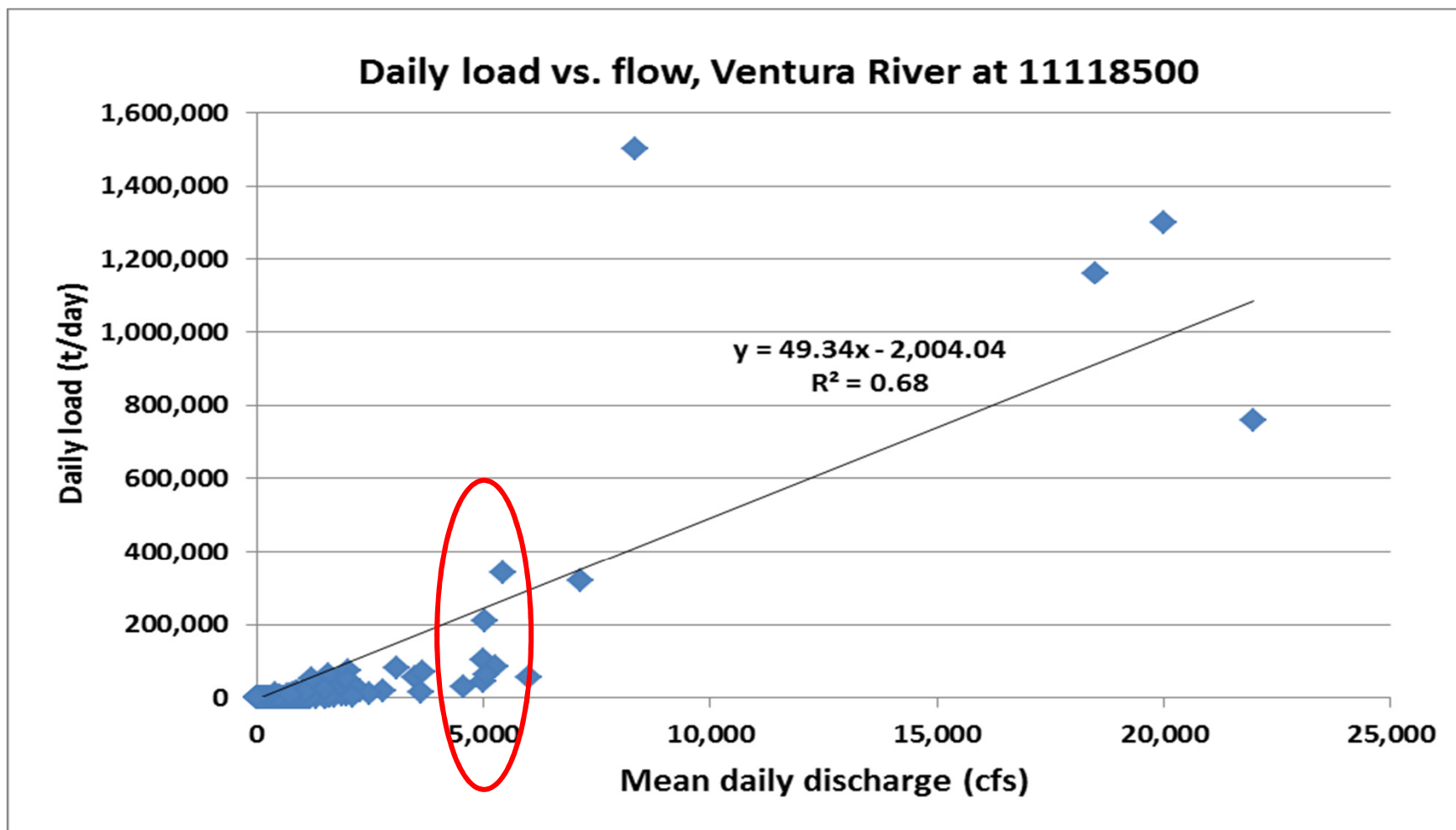
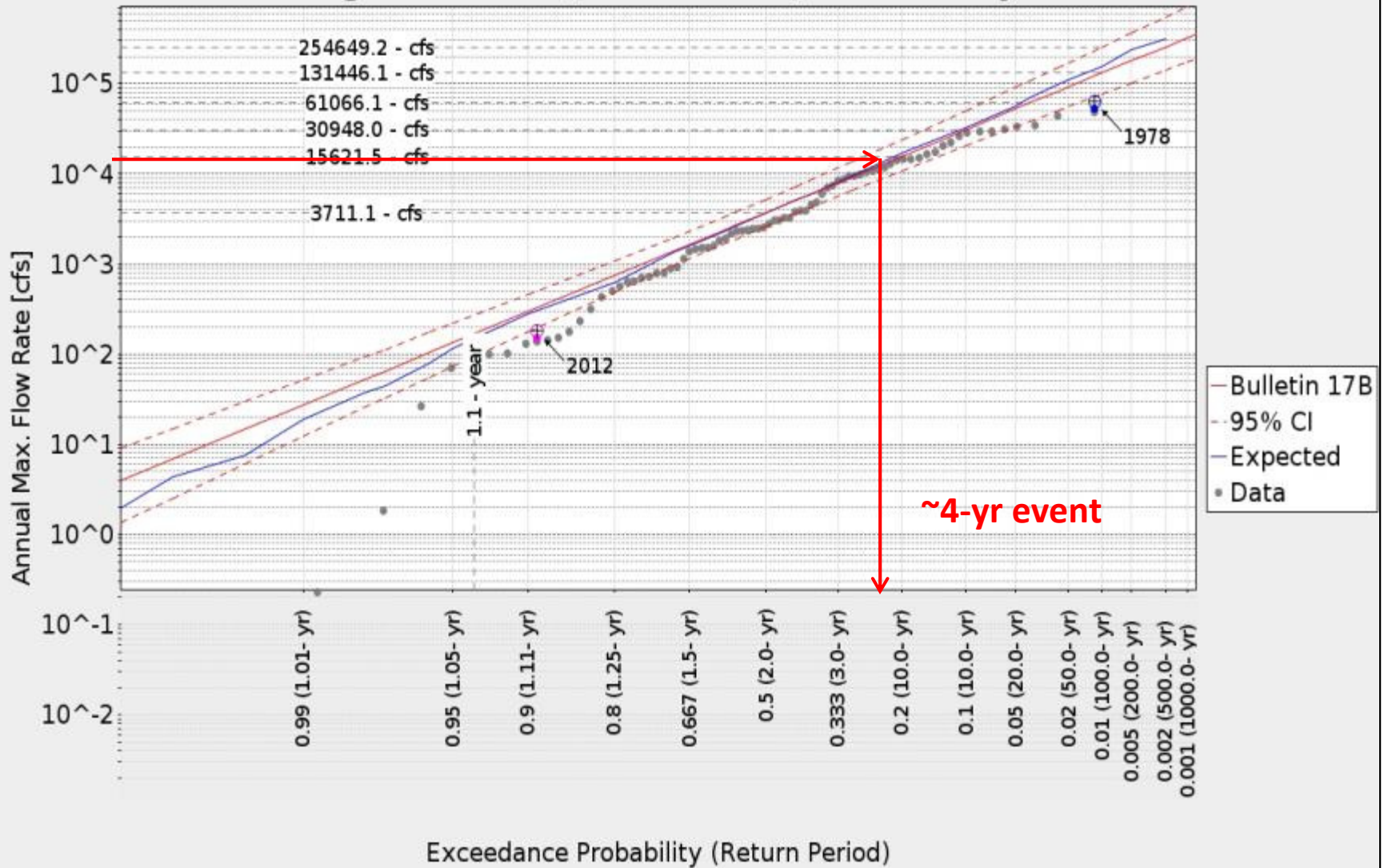


Figure 5. Comparison of mean daily (water) discharges and daily suspended sediment loads on the Ventura River at gage 11118500 for the period 1969-1989.

11118500-VENTURA R NR VENTURA Agency: USGS Weighted Skew (G=-0.41055) Probability Plot



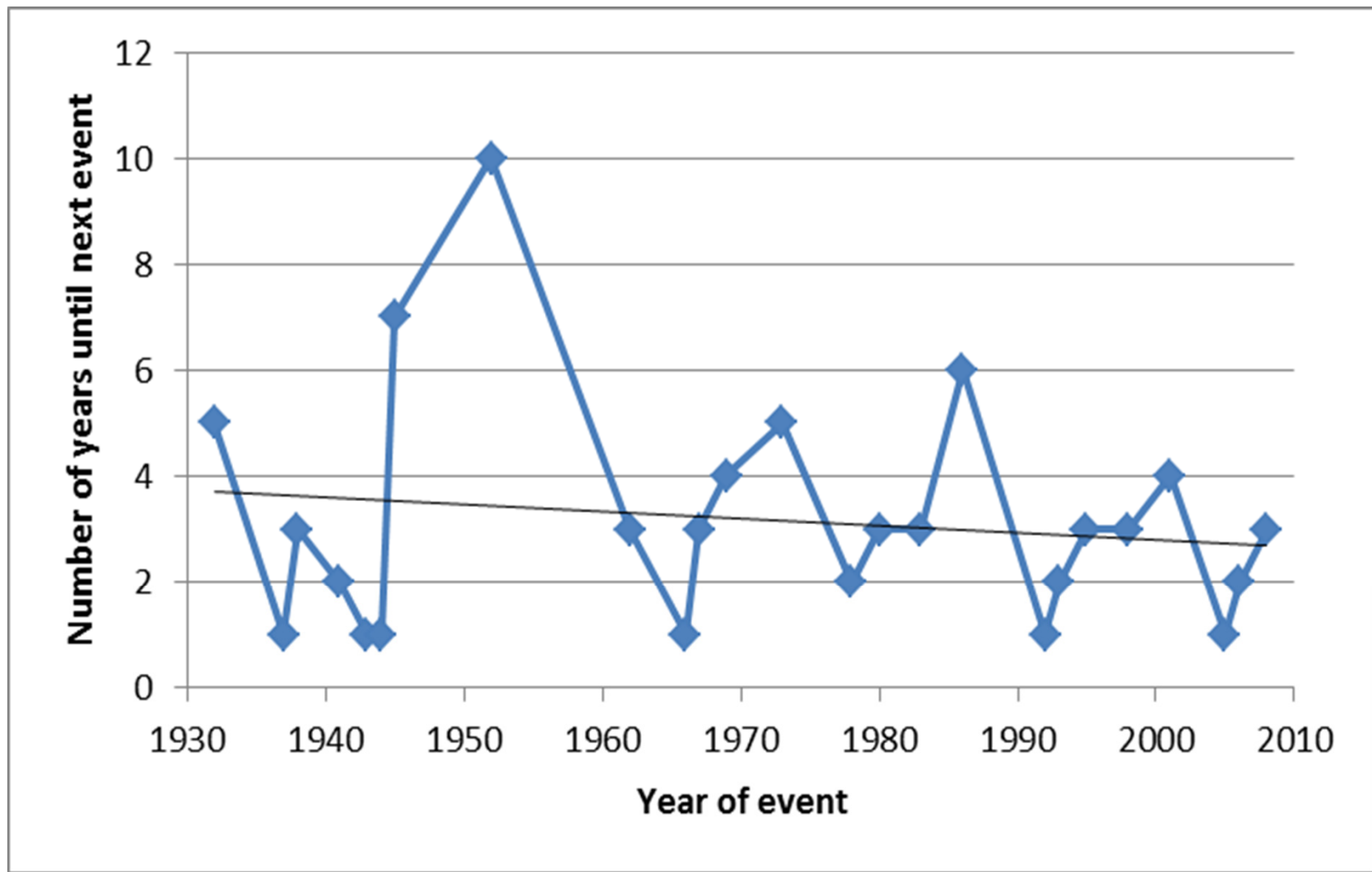


Figure 8. Time series of “events” (average daily flow of $\geq 5,000$ cfs at 1118500 and/or $\geq 1,667$ cfs in Matilija Creek) plotted on the y-axis as the number of years until the next year with at least one such event. Multiple events within the same water year are ignored.

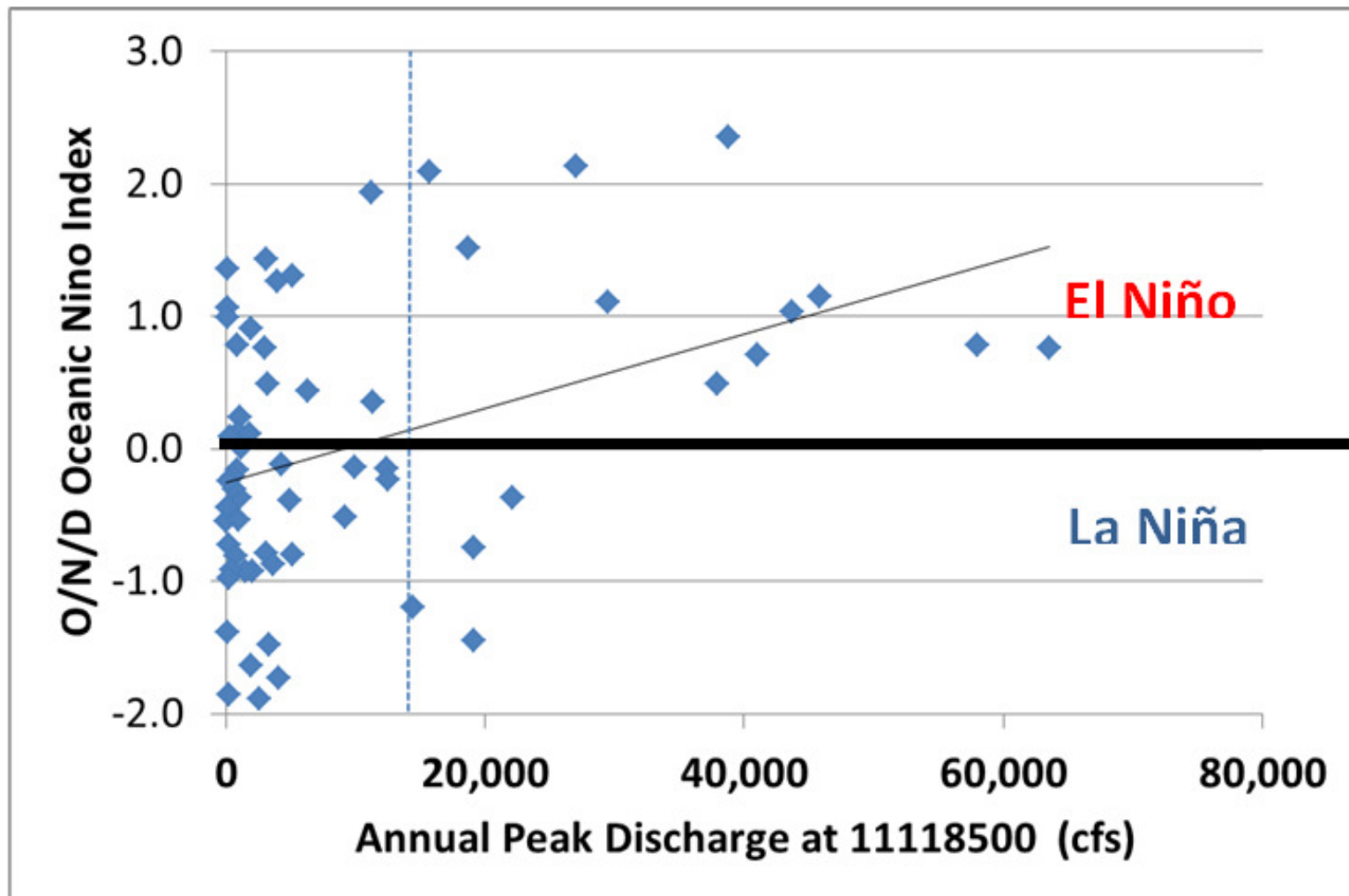


Figure 9. Annual peak discharge on the Ventura River at gage 1118500 plotted against the averaged value of the Oceanic Niño Index for the months of October, November, and December at the beginning of the corresponding water year (data range 1950–2011). The dashed vertical line marks 14,000 cfs, the presumptive peak discharge required for “significant” sediment transport (see text); the thin gray line marks the linear trend of the entire data set.

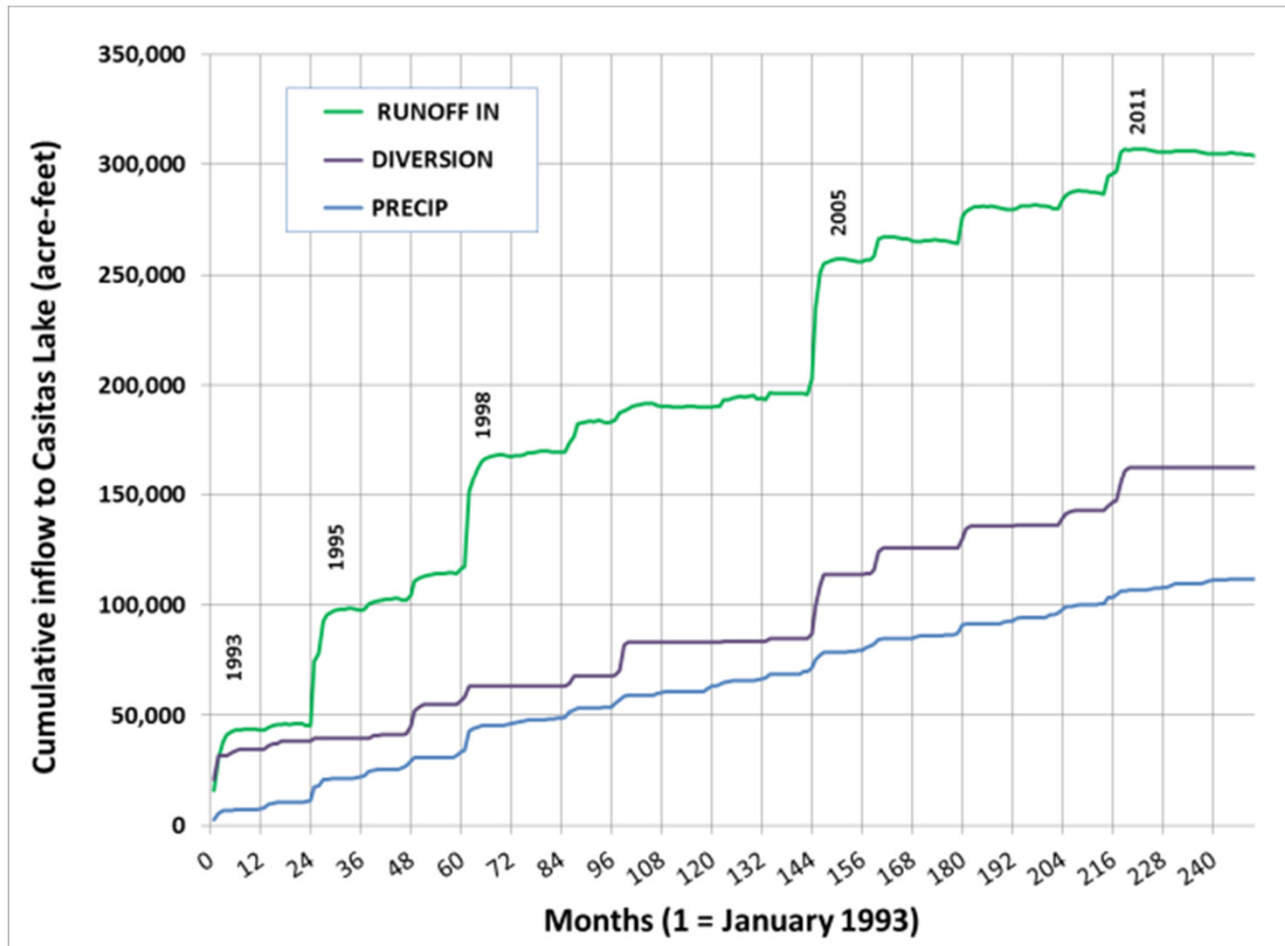


Figure 11. Cumulative volumes of water inputs to Lake Casitas, based on daily records from the Casitas Water District beginning in January 1993. “Runoff in” is derived from the watershed directly draining to the reservoir, and it includes some small negative values presumably resulting from seepage losses. Precipitation was calculated as the product of daily precipitation and lake surface area; the plotted diversion is the record of water inputs from Robles Diversion.

SOURCE	Acre-ft, 1993–2013	Percent of total
Runoff from the reservoir watershed	303,271	52.5%
Robles Diversion from the Ventura River	162,824	28.2%
Direct precipitation on the lake surface	111,867	19.4%
TOTAL	577,962	100.0%

Figure 11. Cumulative volumes of water inputs to Lake Casitas, based on daily records from the Casitas Water District beginning in January 1993. “Runoff in” is derived from the watershed directly draining to the reservoir, and it includes some small negative values presumably resulting from seepage losses. Precipitation was calculated as the product of daily precipitation and lake surface area; the plotted diversion is the record of water inputs from Robles Diversion.

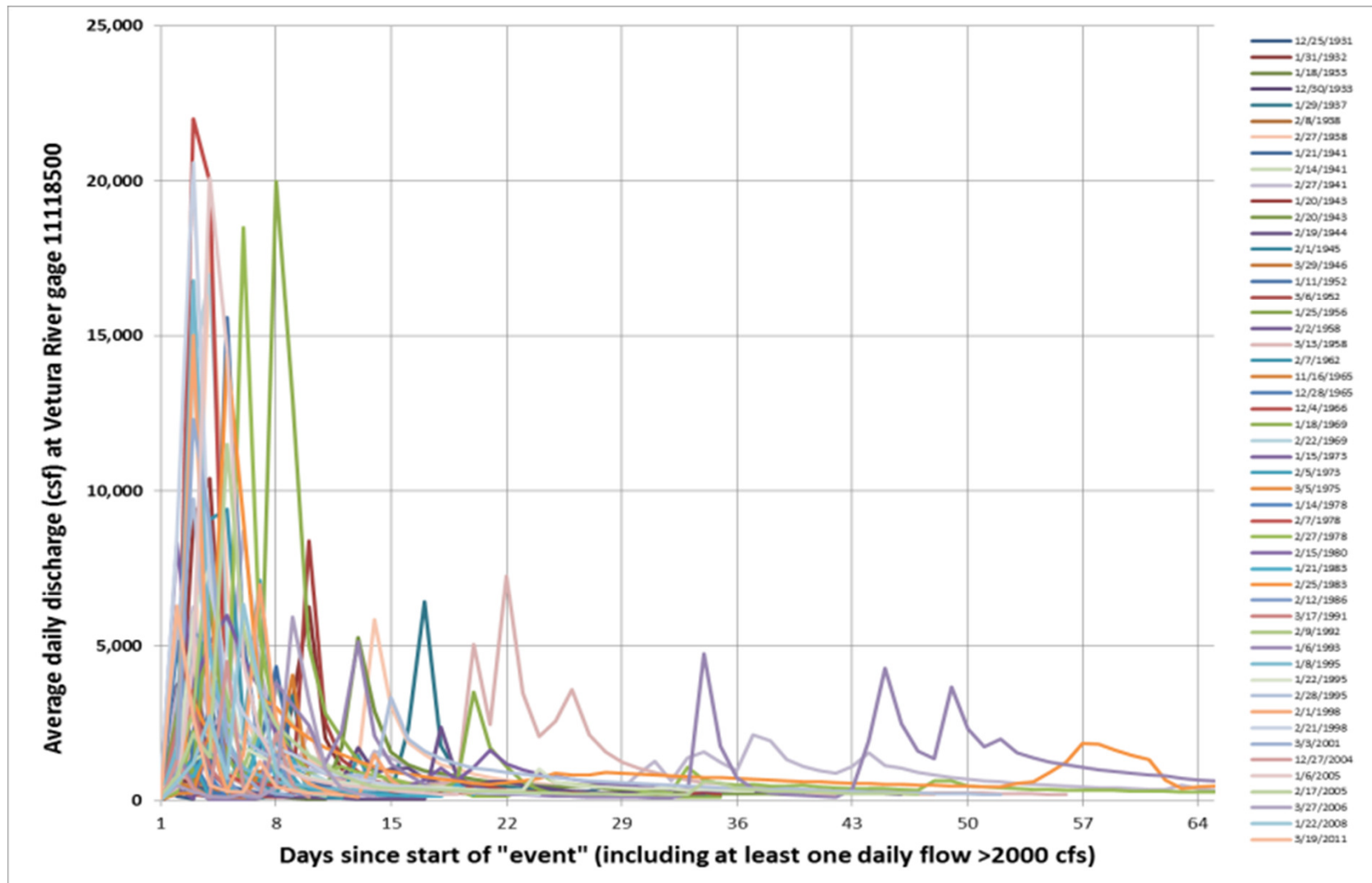


Figure 15. Hydrographs of all flow events on the Ventura River at gage 11118500 for the entire period of record. An “event” is defined as a continuous period of flows including at least one daily average flow >2,000 cfs; the graphed period is extended both prior to and following that >2,000 cfs discharge to include all “adjacent” days with flows above 200 cfs.

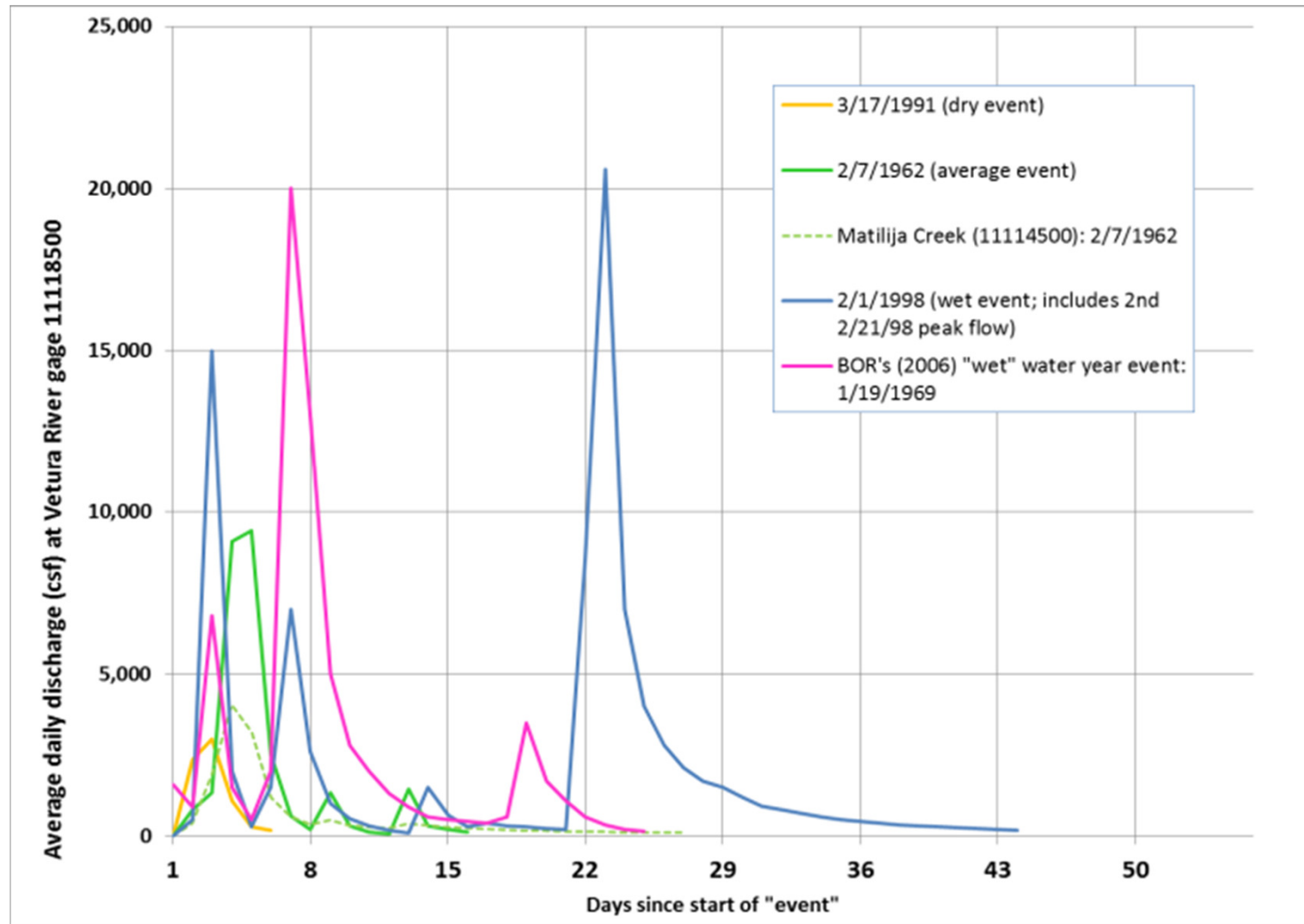


Figure 17. Hydrographs of the representative flow events identified in Figure 16. For comparison, the same-day flows for the “average” event on Matilija Creek (gage 11114500) are also plotted, showing the typical ~1:3 ratio with peak flows with the Ventura River and close correspondence in timing (Matilija gages were not operational during the “dry” and “wet” events).

Topics

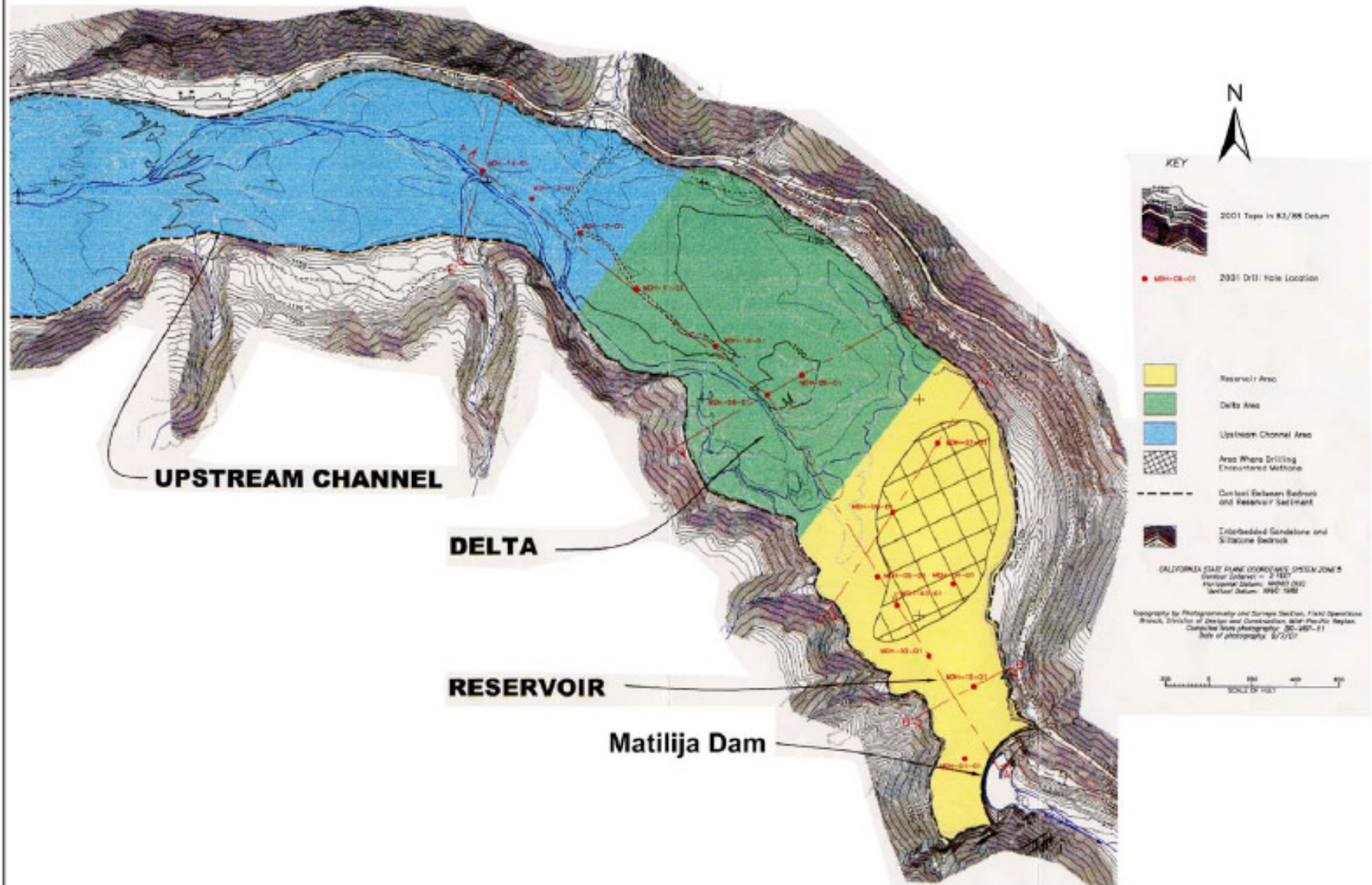
1. Watershed hydrology
- 2. Impoundment-area sediment**
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MATILIJA DAM
DAM REMOVAL PLANS AND SEDIMENT TRANSPORT ANALYSIS AND ROBLES DIVERSION MITIGATION



Geotechnical Investigations



From Appendix C of Geotechnical Report

Example boring log from Appendix C (MDH-03-01)

GEOLOGIC LOG OF DRILL HOLE NO. MDH-03-01

SHEET 2 OF 2

FEATURE: MATILDA DAM ECOSYSTEM RESTORATION FEASIBILITY STUDY
 LOCATION: Matilda Reservoir
 BGLIN: 82151 FINISHED: 8/22/01
 DEPTH AND ELEVATION OF WATER LEVEL:
 AND DATE MEASURED: 8.0 (1088.2) 06/21/2001

PROJECT: VENTURA RIVER PROJECT
 COORDINATES: N 2,082,047.5 E 6,156,896.8
 TOTAL DEPTH: 68.3
 DEPTH TO BEDROCK: Not Encountered

STATE: CALIFORNIA
 WATER ELEVATION: 1088.9
 ANGLE FROM HORIZONTAL: 90 AZIMUTH:
 HOLE LOGGED BY: Mike McCarty
 REVIEWED BY: Joel Starn

NOTES	DEPTH	CORE RECOVERY	LABORATORY DATA										TOXICITY SAMPLES	ORGANIC LIMIT SYMBOL	VISUAL CLASSIFICATION	ELEVATION	CLASSIFICATION AND PHYSICAL CONDITION	
			% Fines	% SAND	% GRAVEL	LIQUID LIMIT	PLASTICITY INDEX	% ORGANIC	COHESION	LAB	TEMPERATURE	SATURATION						
ESTIMATED DRILLING FLUID RETURN: None used; advanced hole with flight augers. Reservoir water was added to the inside of the flight augers each time the 5 ft. sample barrel was retrieved to keep sand from running in. CASING RECORD: Casing Size: Casing Depth Interval Drilled 3-3/4" PA 0.0 - 68.3 ft. 0.0 - 68.3 ft. REASON FOR HOLE TERMINATION: The hole was terminated for safety reasons upon encountering large quantities of pressurized methane gas at a depth of 68.3 ft. HOLE COMPLETION: As the augers were pulled the hole was allowed to slough in on itself. DEPTH OF WATER: Date: 06/21/01 Depth of Water: 8.0 ft.	0																	
	10	100															1088.5	58.1 to 62.8 ft. Sandy Silty sML : About 90% fines with low to no plasticity, slow to rapid disintegration, high dry strength, about 40% fine sand; maximum size, fine sand; moist, gray, soft; about 15% 1 to 2 mm diameter methane gas bubbles in the sediment from 58.8 to 62.1 ft.; strong reaction with HCl.
	40	100	48	51	0	MP	MP	NA	SM								1088.8	62.8 to 68.3 ft. SS ML : About 90% fines with medium plasticity, slow disintegration, high dry strength; about 10% fine sand; trace organic; maximum size, fine sand; moist, gray, soft; plant roots at 68.2 ft.; pressurized methane pocket at 68.3 ft.; stopped drilling and ended the hole; strong reaction with HCl.
	50	100															1088.9	
	60	100															1089.2	
	70	100															1089.5	
	80	100															1089.8	
	90	100															1090.1	
	100	100															1090.4	
	110	100															1090.7	
	120	100															1091.0	
	130	100															1091.3	
	140	100															1091.6	
	150	100															1091.9	
	160	100															1092.2	
	170	100															1092.5	
	180	100															1092.8	
	190	100															1093.1	
	200	100															1093.4	
	210	100															1093.7	
	220	100															1094.0	
	230	100															1094.3	
	240	100															1094.6	
	250	100															1094.9	
	260	100															1095.2	
	270																	

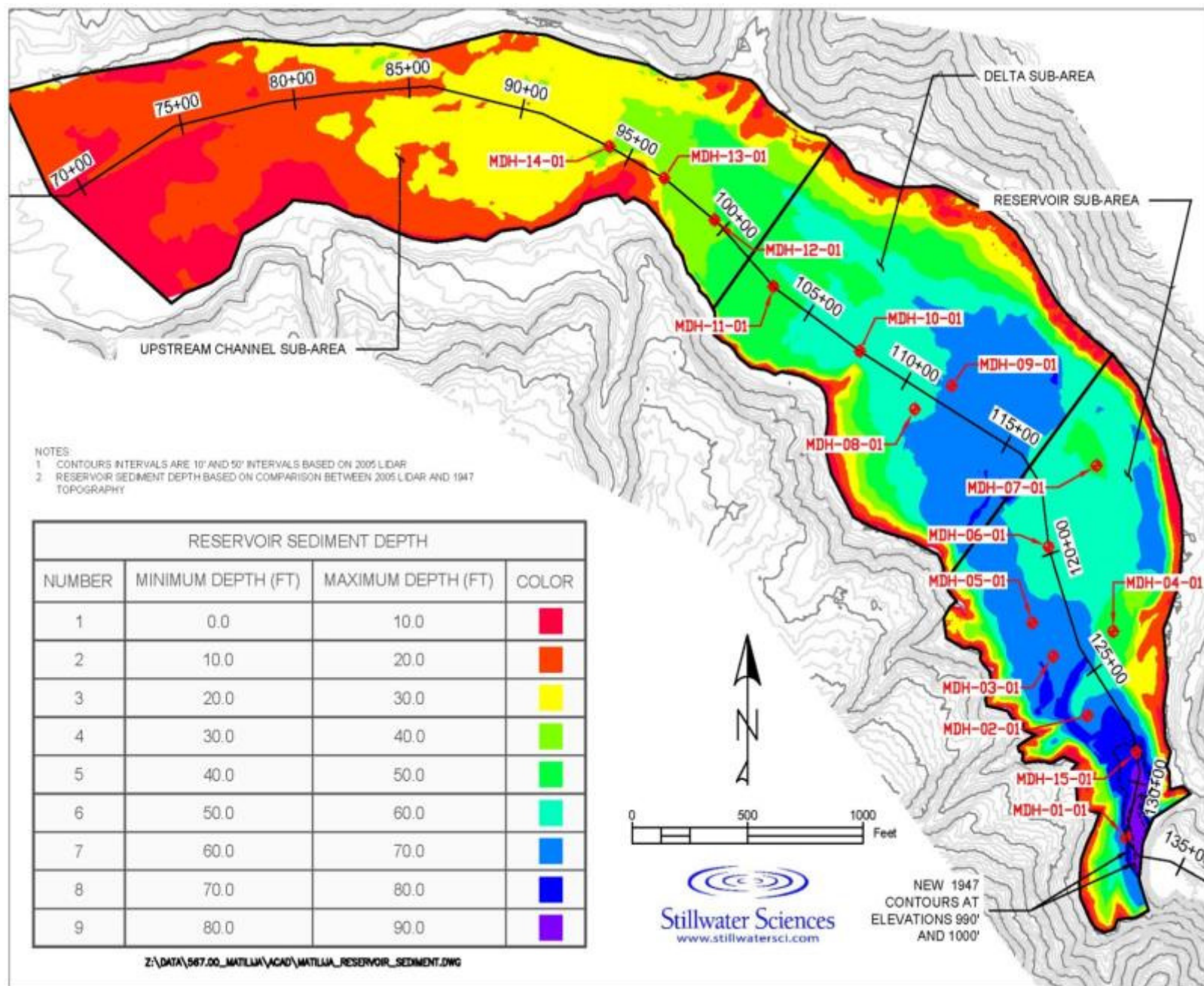


Figure 1. Plan view of Matilija Reservoir sediment deposits and borehole locations.

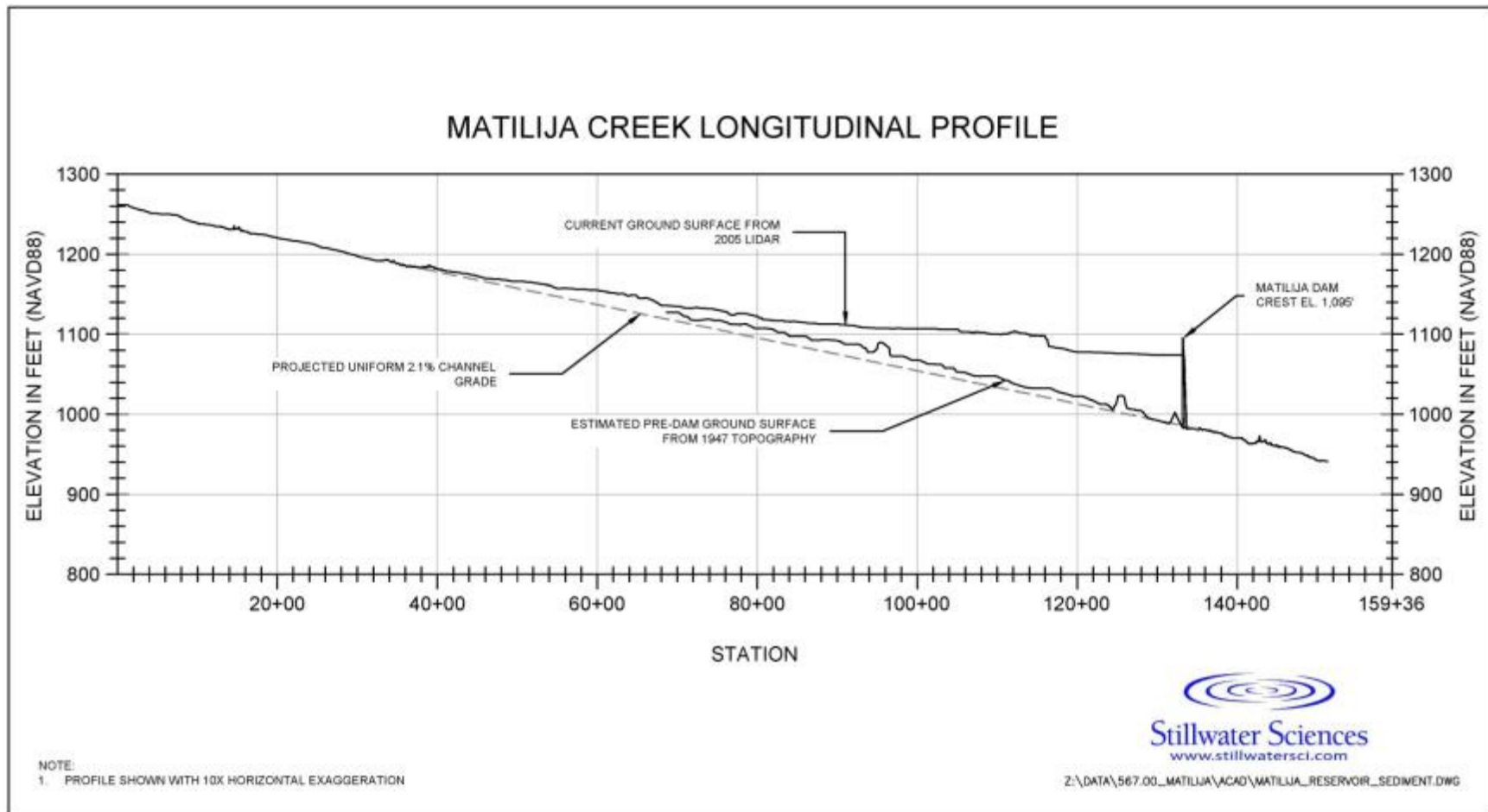


Figure 2. Matilija Creek longitudinal profile.

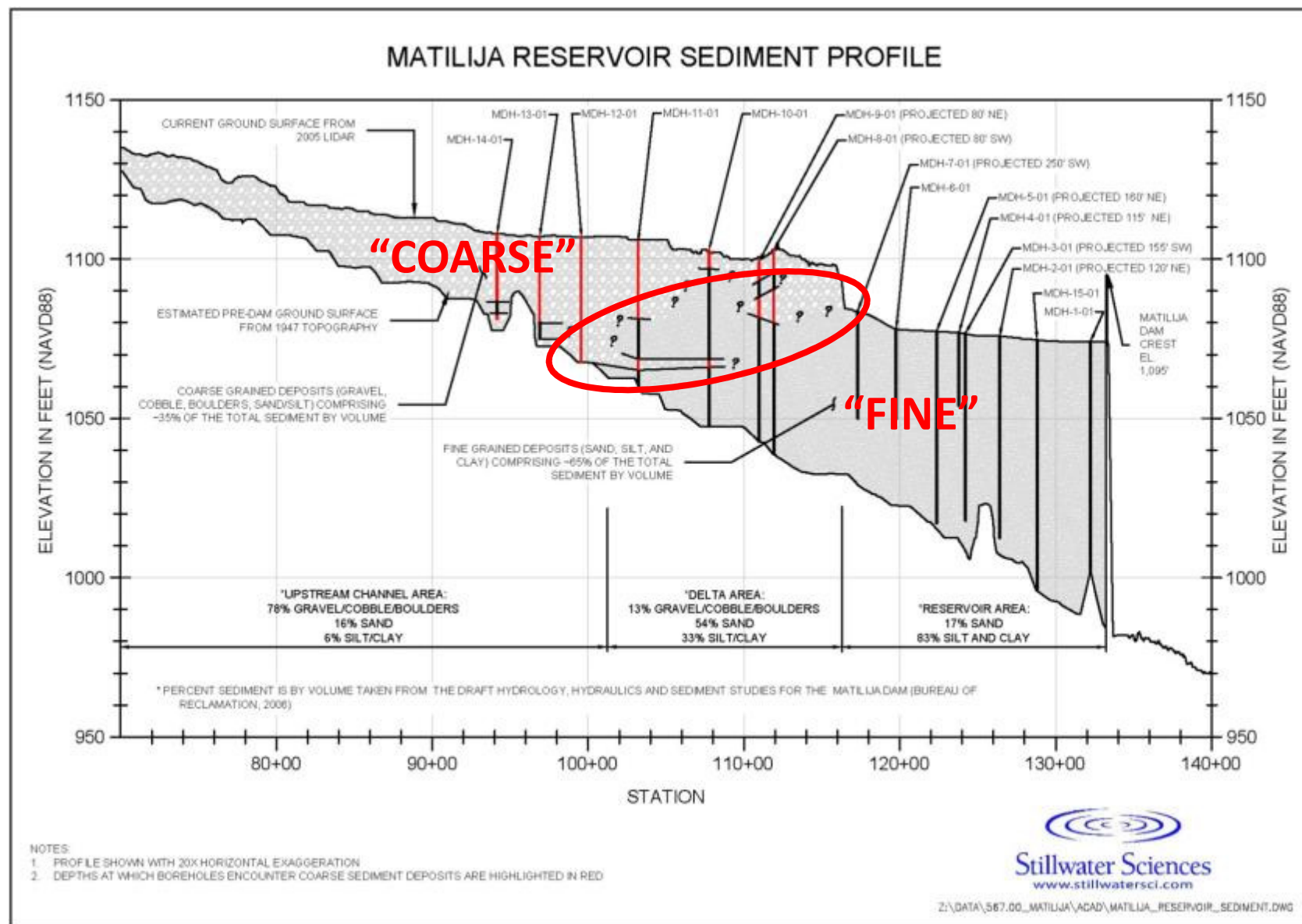


Figure 3. Matilja Reservoir sediment deposit profile.

Table 1. Sediment gradation percentages (determined from BOR 2006, Table 5.6).

Sediment Deposit Sub-Area:	% Gravel (>2 mm)	% Sand (0.0625–2 mm)	% Silt/Clay (<0.0625 mm)
Reservoir	0%	17%	83%
Delta	13%	54%	33%
Upstream Channel	78%	16%	6%

Table 2. Sediment gradation volumes.

Sediment Deposit Sub-Area	Total Volume Sediment (as of 2005)	Volume Gravel (>2 mm)	Volume Sand (0.0625 - 2 mm)	Volume Silt/Clay (<0.0625 mm)
	(all values in cubic yards)			
Reservoir	2,420,000*	0	410,000	2,010,000*
Delta	3,230,000	420,000	1,740,000	1,070,000
Upstream Channel	1,150,000	900,000	180,000	70,000
Total Volume	6,800,000*	1,320,000	2,330,000	3,150,000*
Total Percent	100%	19%	35%	46%

*Inferred deposition of silt/clay in the Reservoir sub-area during the period 2002–2005 but not “seen” by the LiDAR or 2001 boreholes should raise these amounts by ~160,000 yd³ (see below).

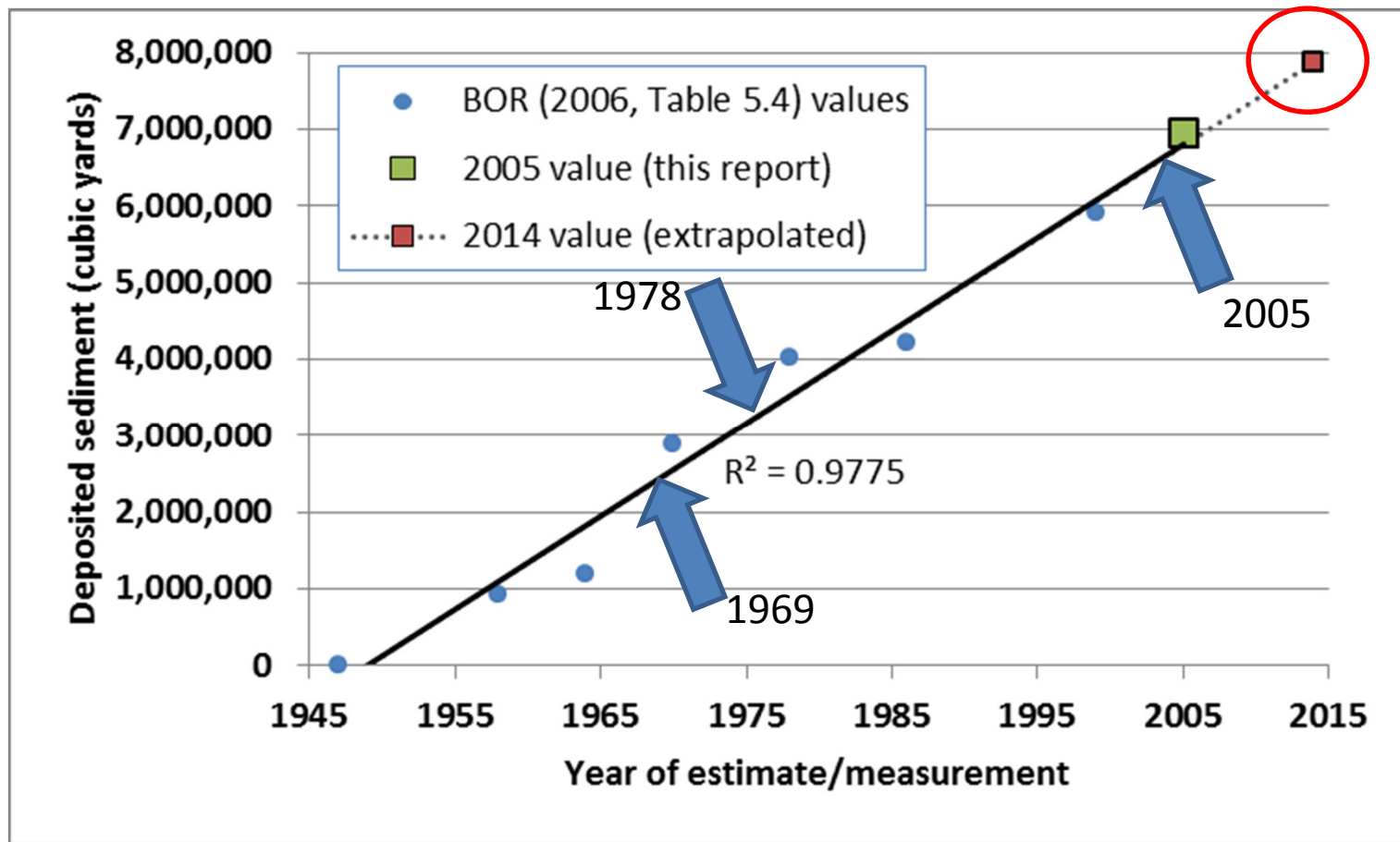


Figure 4. Historically inferred, measured, and extrapolated sediment volumes behind Matilija Dam (data sources as noted).

CONUNDRUM #1: Why so little effect from the really big flow events?

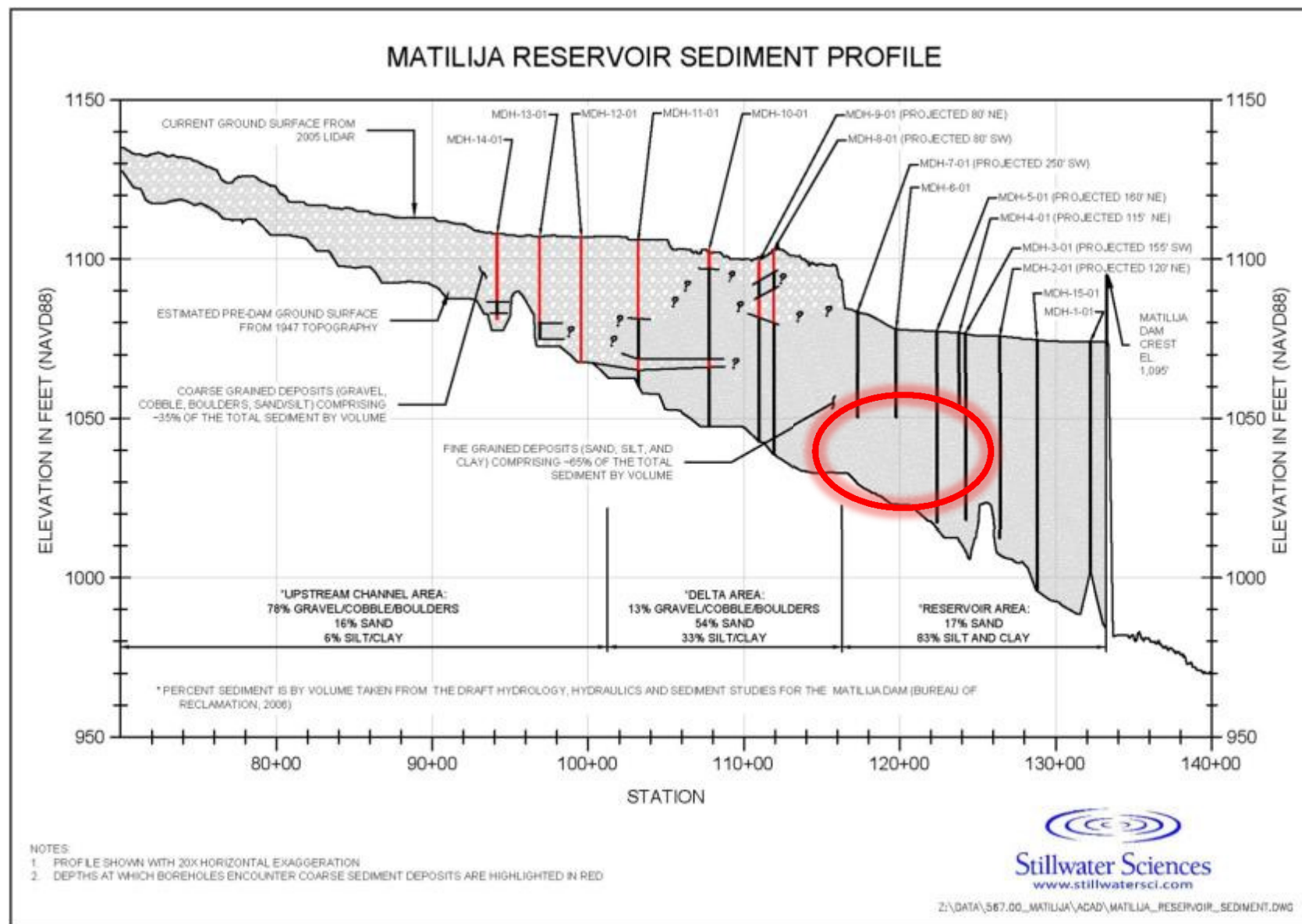
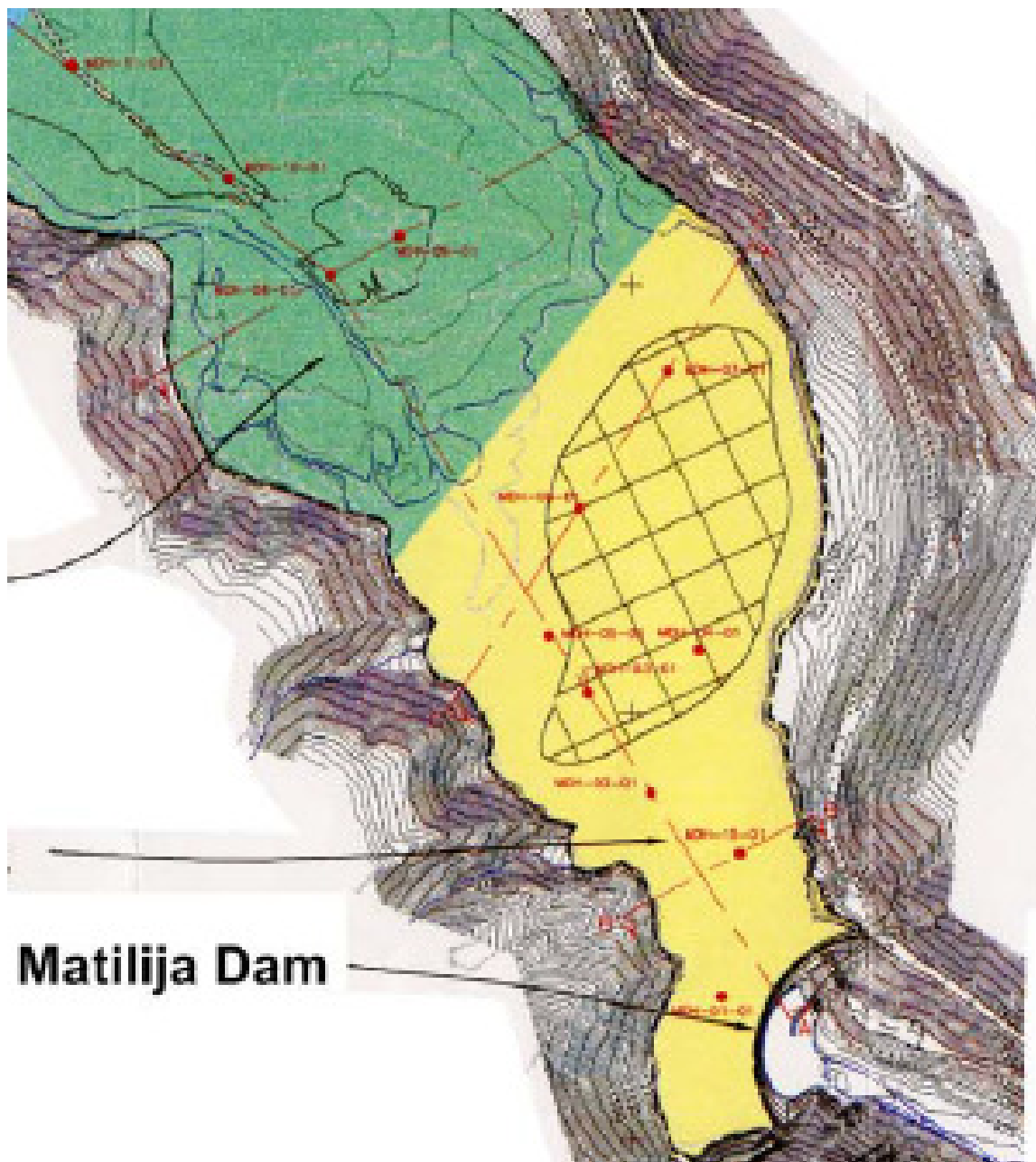


Figure 3. Matilja Reservoir sediment deposit profile.



● MBH-01-01 2001 Drill Hole Location



Reservoir Area



Delta Area



Upstream Channel Area



Area Where Drilling
Encountered Methane



Contact Between Bedrock
and Reservoir Sediment



Interbedded Sandstone and
Siltstone Bedrock

CALIFORNIA STATE PLANE COORDINATE SYSTEM, ZONE 9

Contour Interval = 2 Feet

Horizontal Datum: NAD83 (92)

Vertical Datum: 1988 TIGER

Topography by Photogrammetry and Survey Section, Field Operations
Branch, Division of Design and Construction, South Pacific Region
Computer Aided Photography: 30-280-01
Date of photography: 6/7/01



Matilija Dam

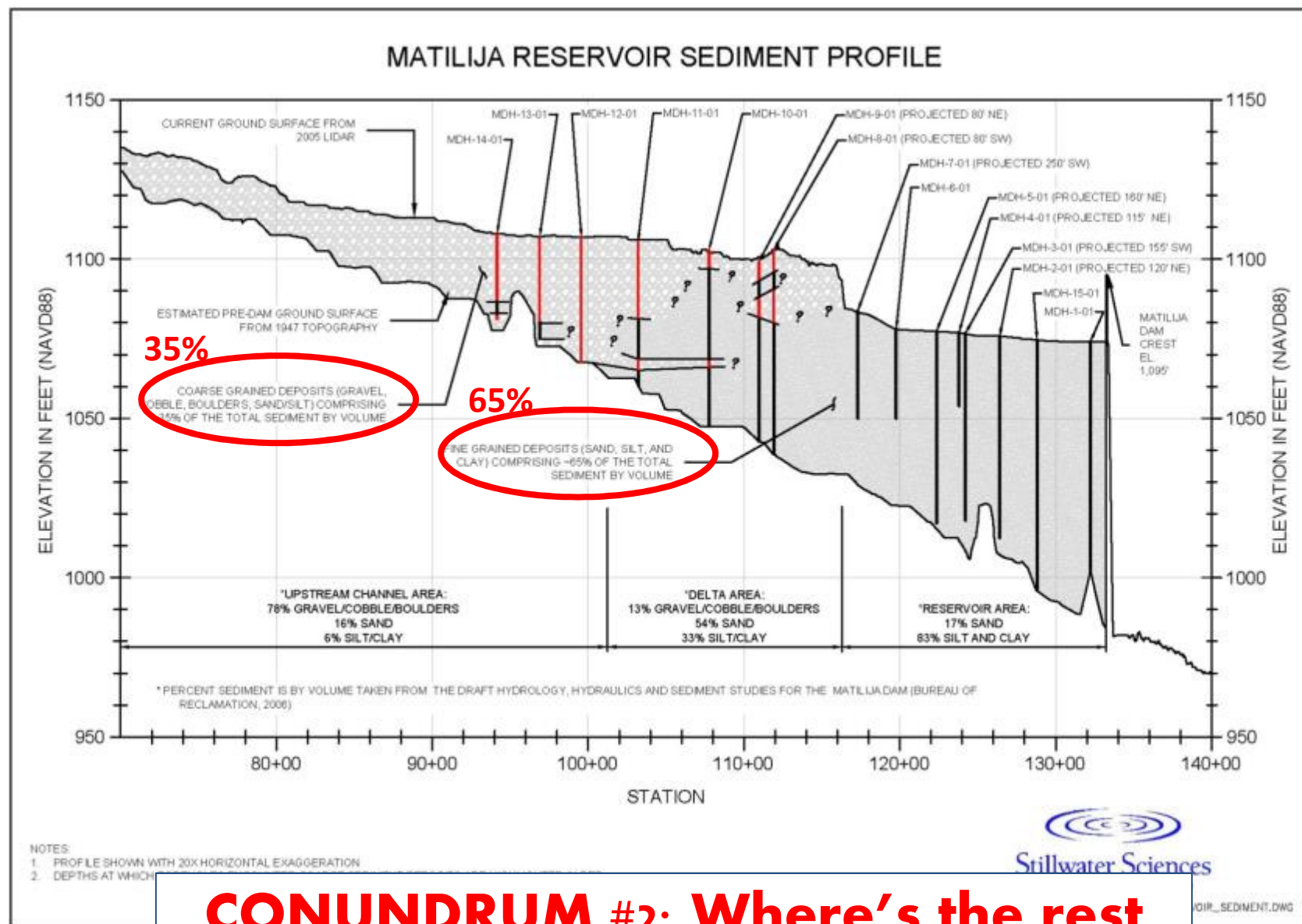


Figure 3.

CONUNDRUM #2: Where's the rest of the fine sediment?



Topics

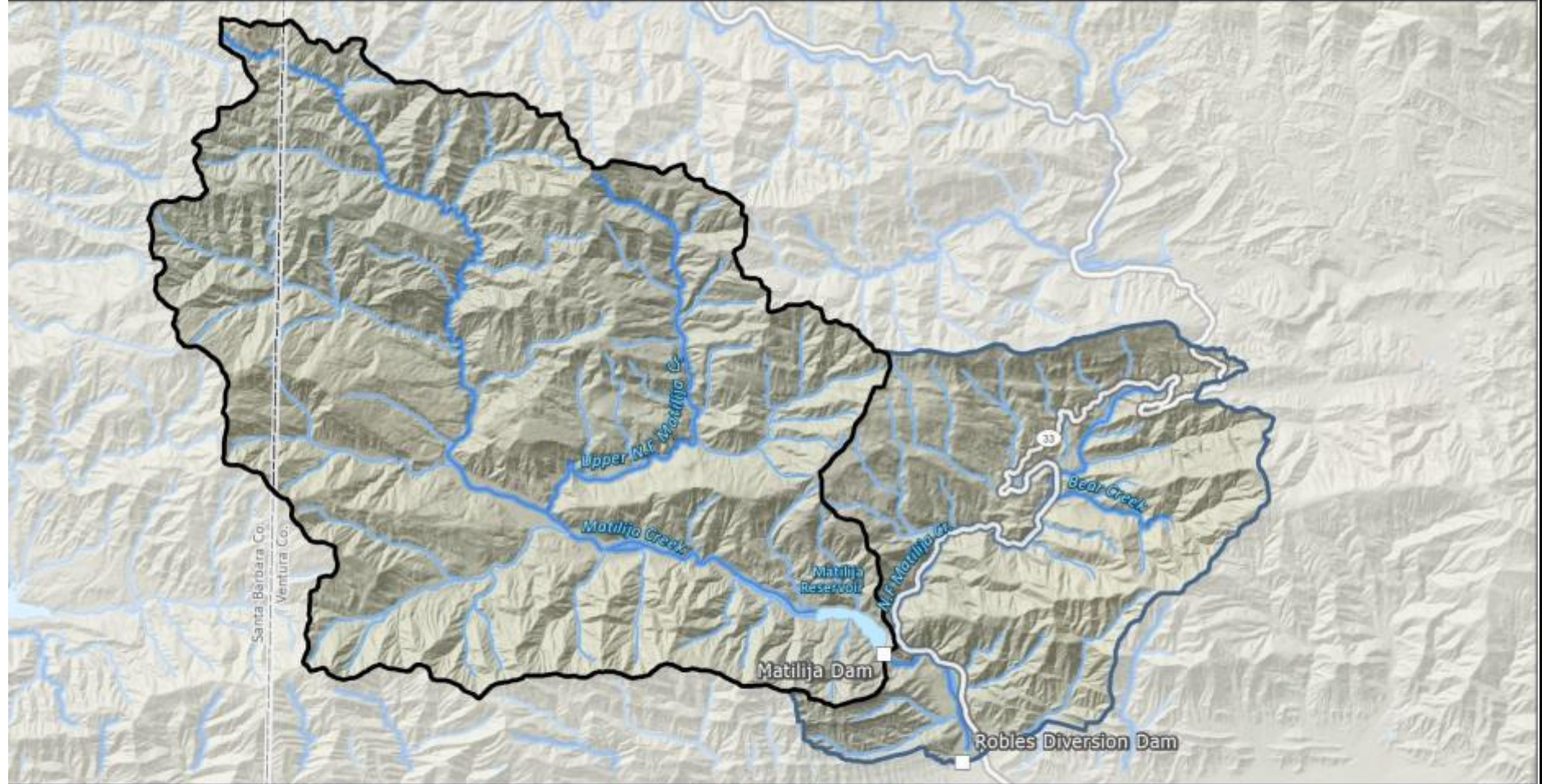
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MATILIJA DAM
DAM REMOVAL PLANS AND SEDIMENT TRANSPORT ANALYSIS AND ROBLES DIVERSION MITIGATION



MATILAJA DAM REMOVAL ANALYSIS & MITIGATION

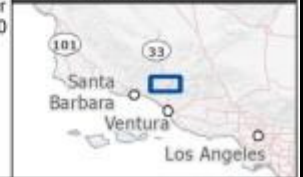


Map

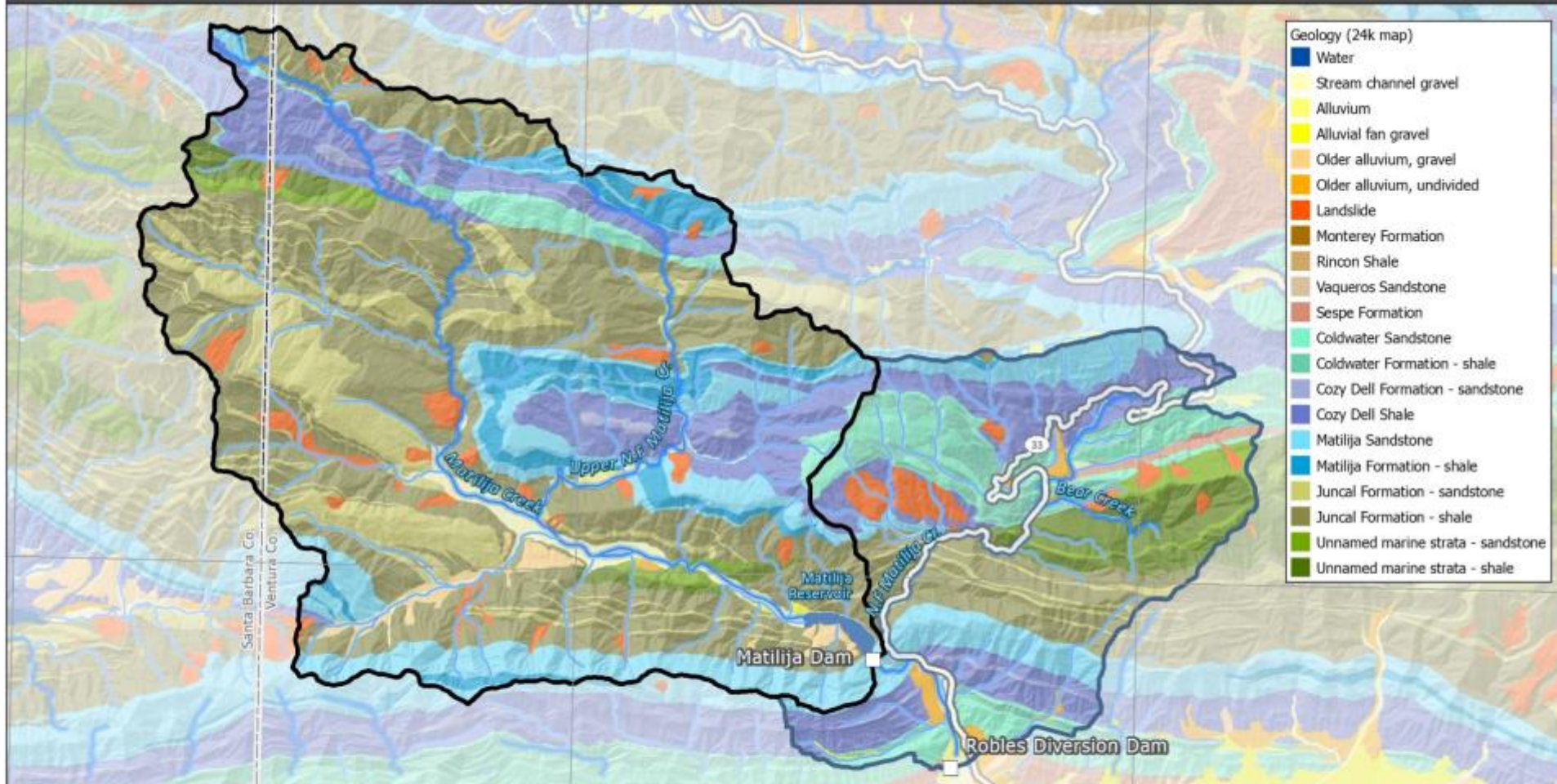
- Dam
- Matilija Basin
- Major channels
- North Fork Matilija Basin
- Other streams

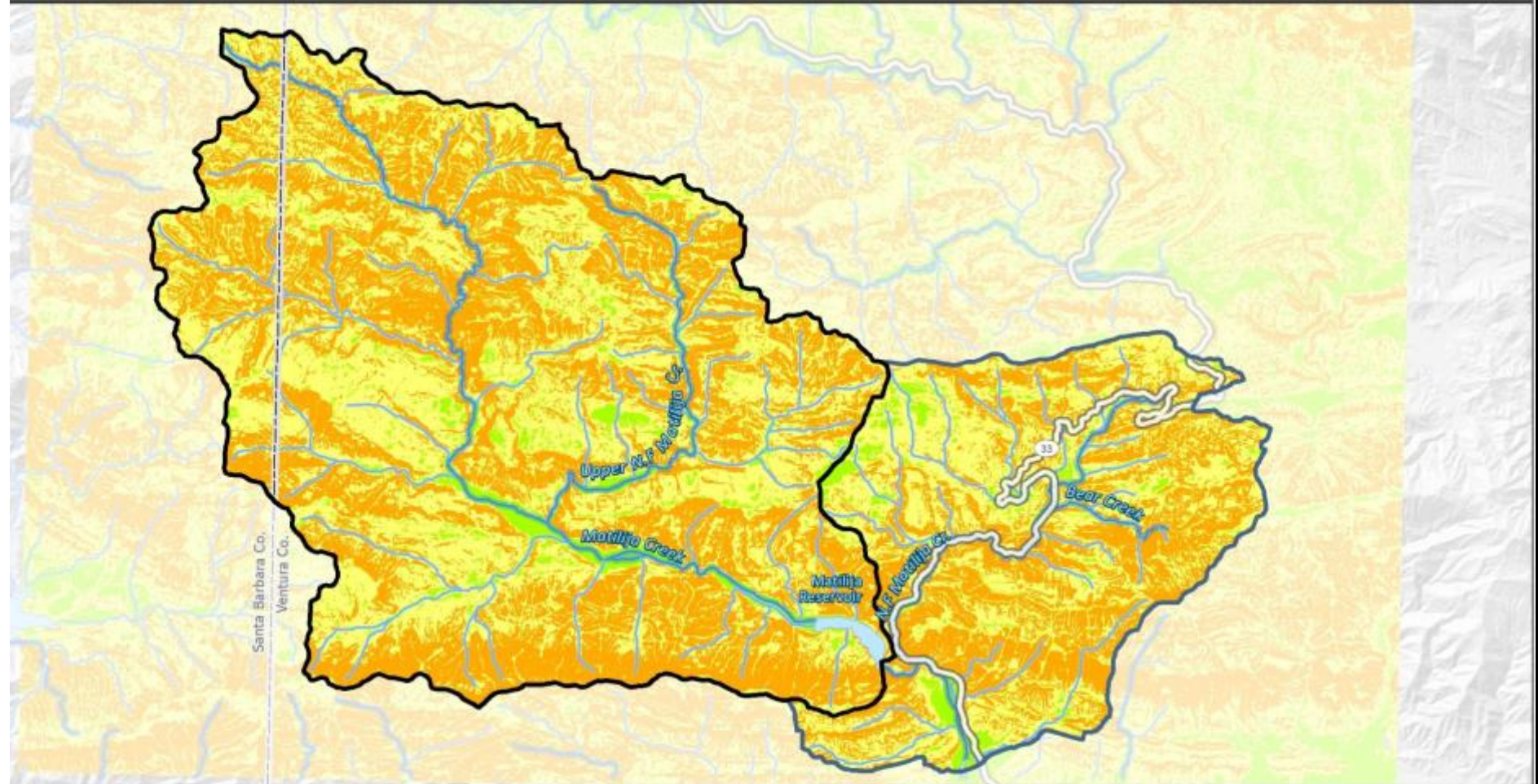
Map Sources:
Basins: CalWater
Roads, Cities, Counties, Rivers: ESRI 2010

Map Location



MATILIJA DAM REMOVAL ANALYSIS & MITIGATION





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Map Sources:
Slope: USGS 10m DEM
Basins: CalWater
Roads, Cities, Counties, Rivers: ESRI 2010



Sullwater Sciences
www.sullwater.com

Map Location

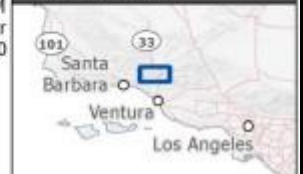


Table 5.14 of BOR (2006) reports the following estimates of watershed sediment yield:

Watershed	Sediment Yield per mi² (acre-ft/mi²/yr)
Ventura Watershed without Casitas Dam and Matilija Dam	2.10
Ventura Watershed with Casitas Dam and Matilija Dam in place (current conditions)	1.36
Ventura Watershed with Casitas Dam in place	1.64
Matilija Creek Watershed	1.92

UNITS:

2.10 acre-ft/mi² /yr =

1 mm landscape lowering/yr =

2,600 tonnes/km²/yr

*A Method for Spatially Explicit
Representation of Sub-watershed Sediment
Yield, Southern California, USA*

**Derek B. Booth, Glen Leverich, Peter
W. Downs, Scott Dusterhoff & Sebastian
Araya**

Environmental Management

ISSN 0364-152X

Volume 53

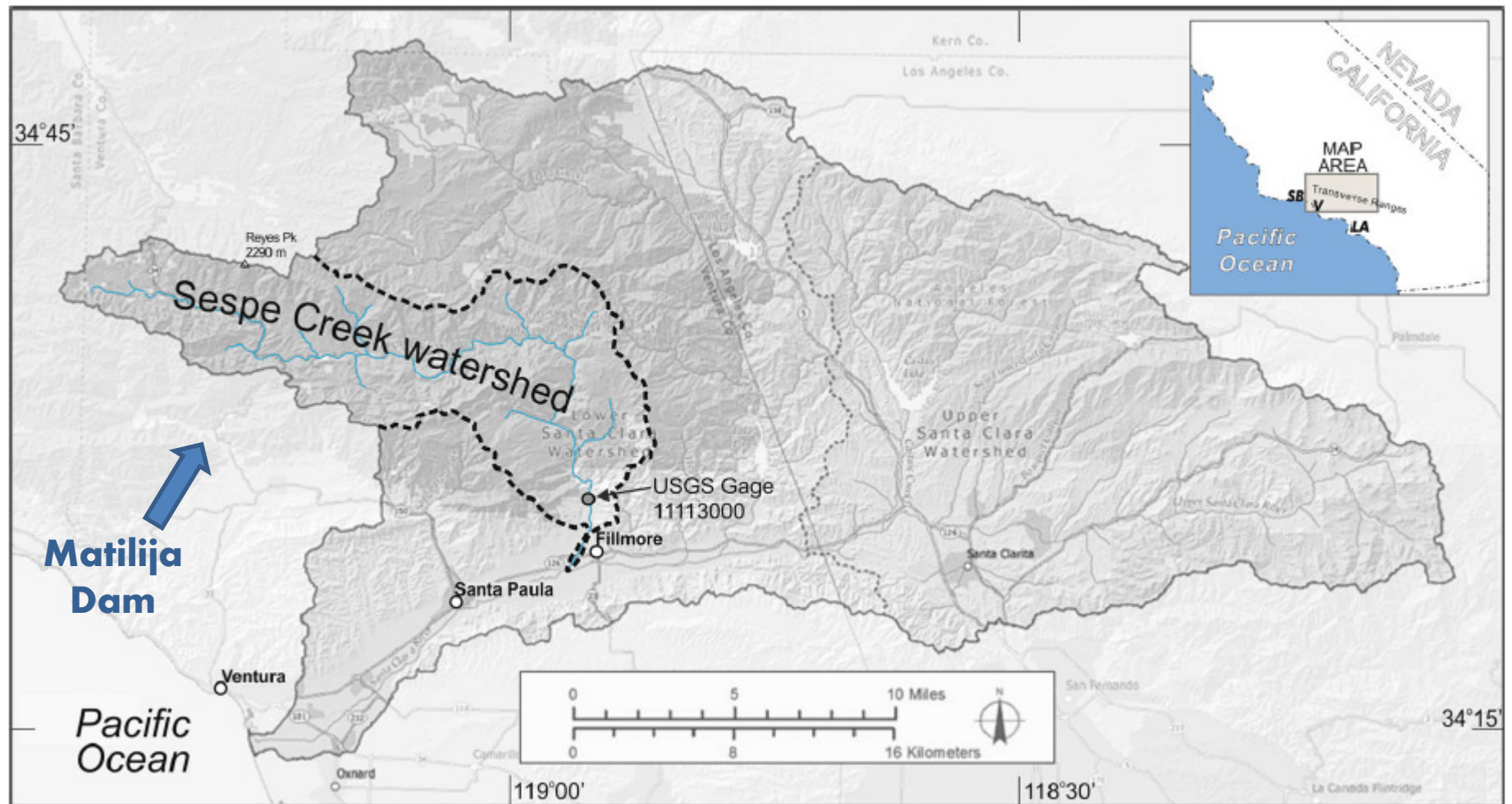
Number 5

Environmental Management (2014)

53:968–984

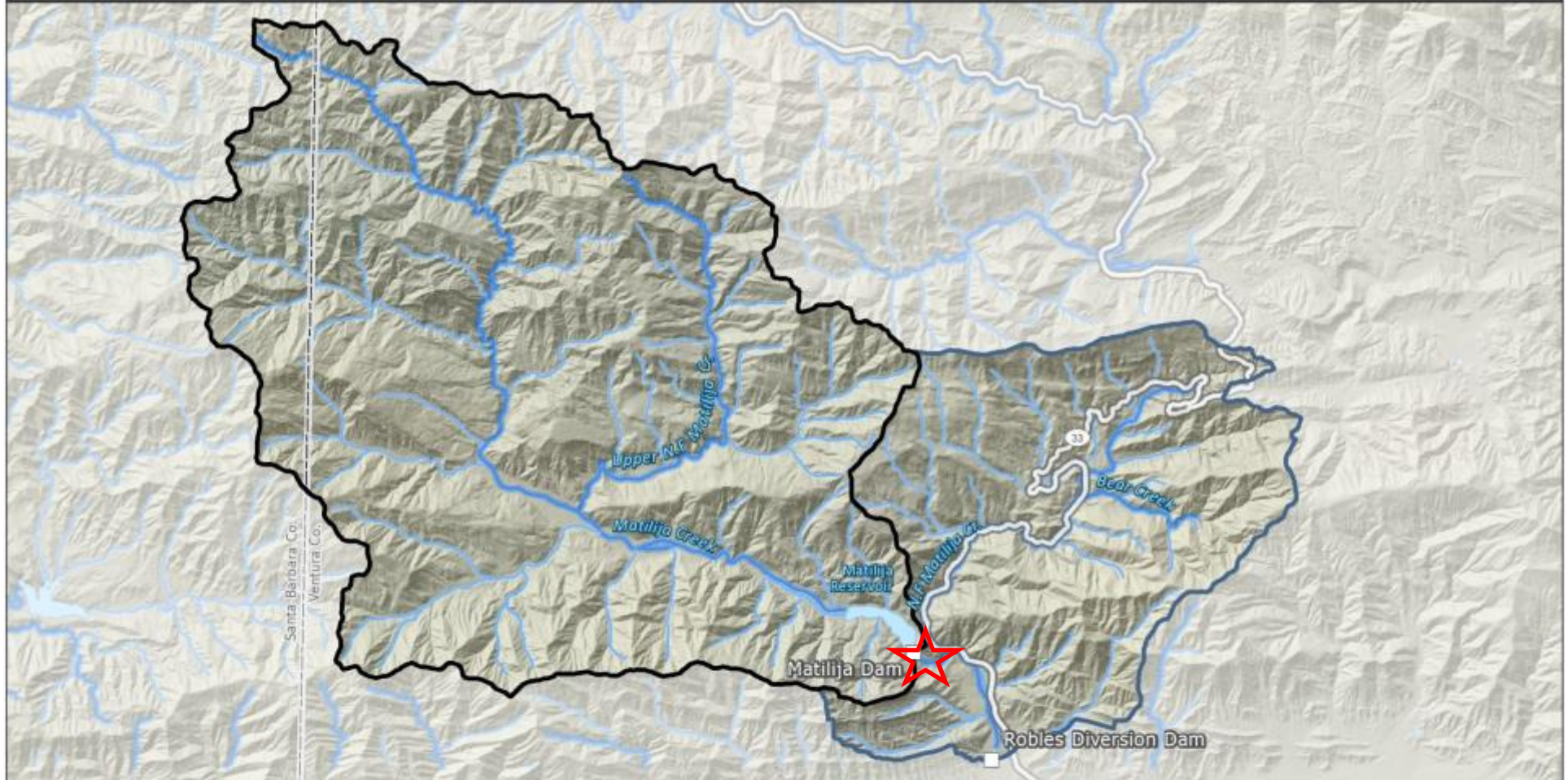
DOI 10.1007/s00267-014-0251-9





Best estimate for Sespe Creek: 2,600 tonnes/km²/yr

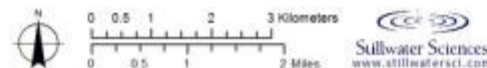
MATILIJA DAM REMOVAL ANALYSIS & MITIGATION



Basemap

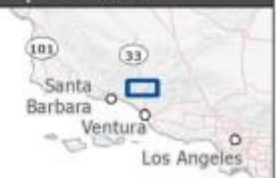
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- Other streams

Map Sources:
Basins: CalWater
Roads, Cities, Counties, Rivers: ESRI 2010



Stillwater Sciences
www.stillwatersci.com

Map Location



Best estimate for Matilija Creek: $3,000 \text{ tonnes/km}^2/\text{yr} = 400,000 \text{ tonnes/yr}$
 (Note: 1 tonne sediment $\approx 1 \text{ yd}^3$, given a density of 1.4 tonnes/m^3)

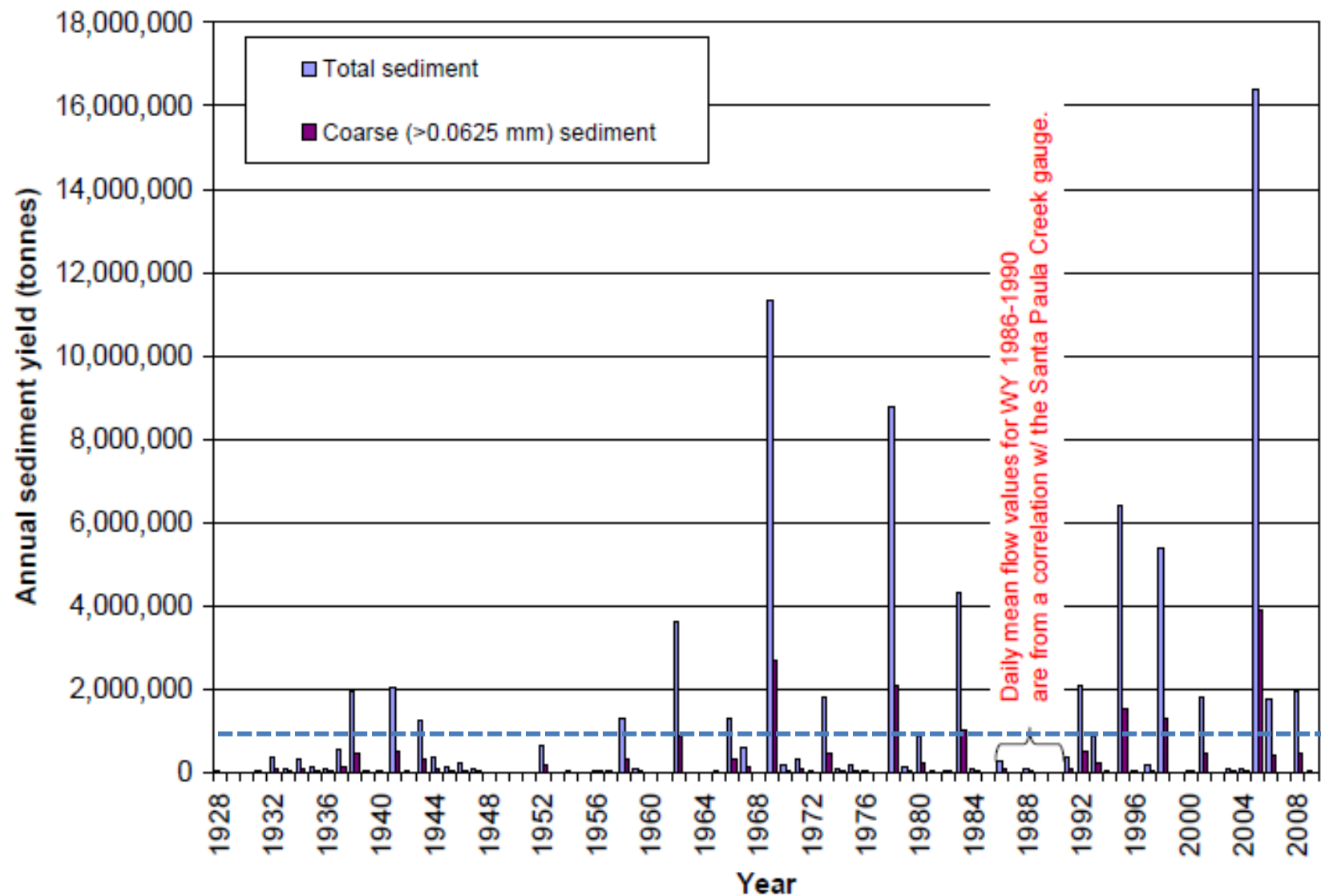
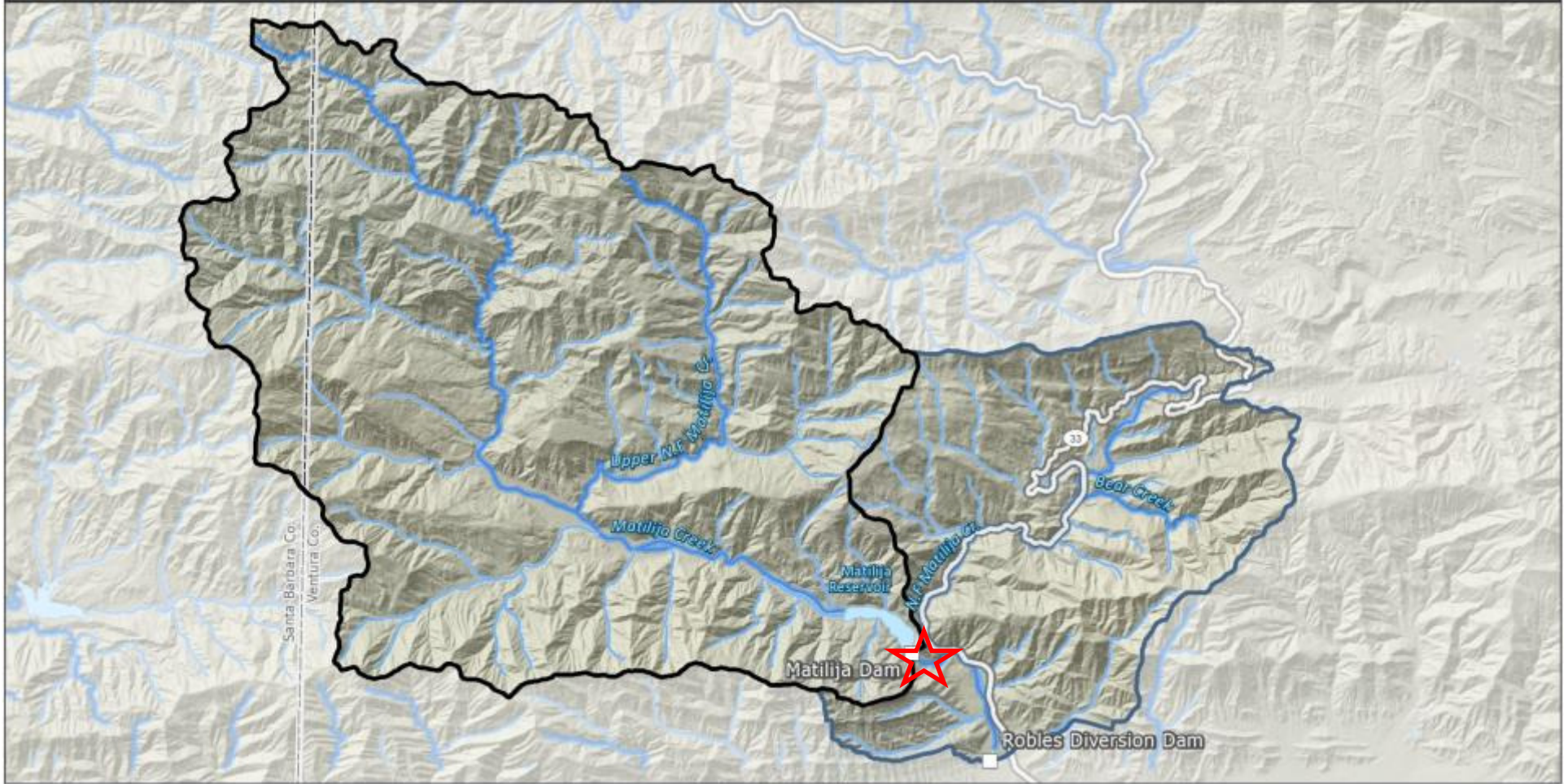


Figure 5. Calculated sediment load for Sespe Creek at Fillmore (USGS gage 11113000). Dashed blue line is the average annual sediment yield calculated from these data (990,000 tonnes/year). Major sediment-yielding years produce two to more than 16 times the long-term average value. From Stillwater Sciences (2010, their Figure 3.2).

MATILIJA DAM REMOVAL ANALYSIS & MITIGATION



- **Average 400,000 tonnes/yr → 1 to >5M yd³ for large events (of which >>50% will be silt/clay) (1-1.5M measured by USGS '69-'87).**
- **Compare this natural single-event transport volume to the ~4M yd³ silt/clay now stored behind the dam.**

Questions?



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